

Nonprehensile Robotic Manipulation: Progress and Prospects

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Laboratory for Intelligent Mechanical Systems
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SpongFest 2012

Major contributors to this talk:

Tom Vose and Paul Umbanhowar

Other contributing colleagues, students, and postdocs:

Adam Barber, Matt Elwin, Bobby Gregg, Yu-Wei Liao,
Andy Long, Matt Mason, Nelson Rosa, Ji-Chul Ryu,
Eric Scheerer, James Solberg

Funding:

National Science Foundation
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International Workshop on Recent Developments in Robotics and Control?

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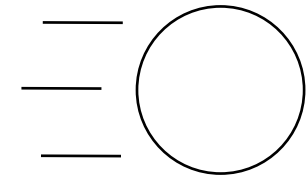
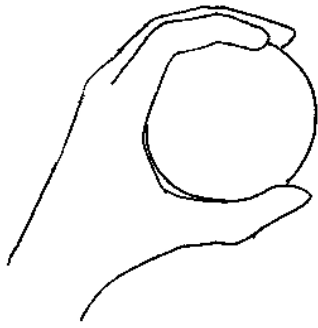
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Nonprehensile Manipulation



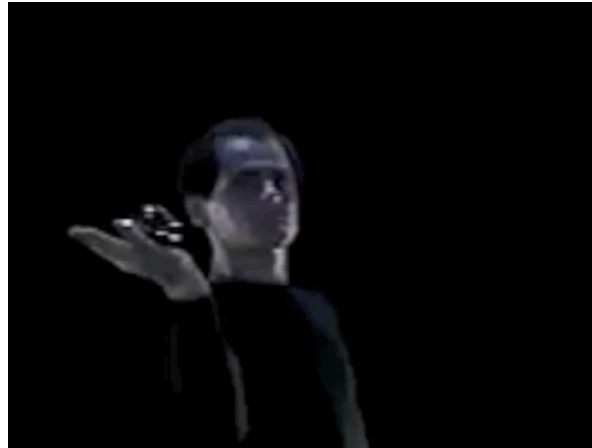
hand controls ball:
prehensile

shared control:
nonprehensile

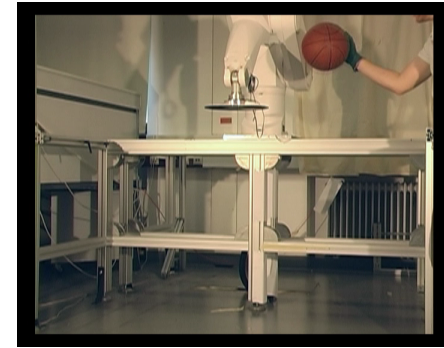
environment
controls ball

form or force
closure grasping

nonprehensile manipulation



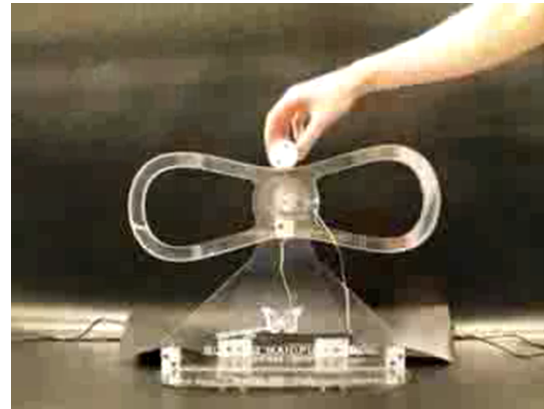
rolling (Michael Moschen)



dribbling
(TU Munich)



throwing and batting
(U Tokyo)



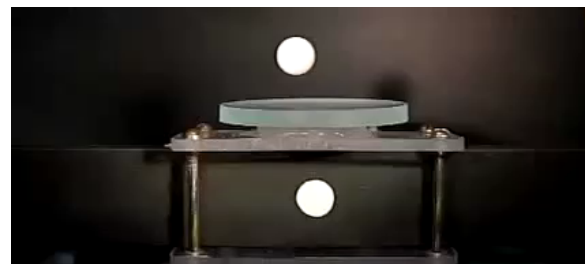
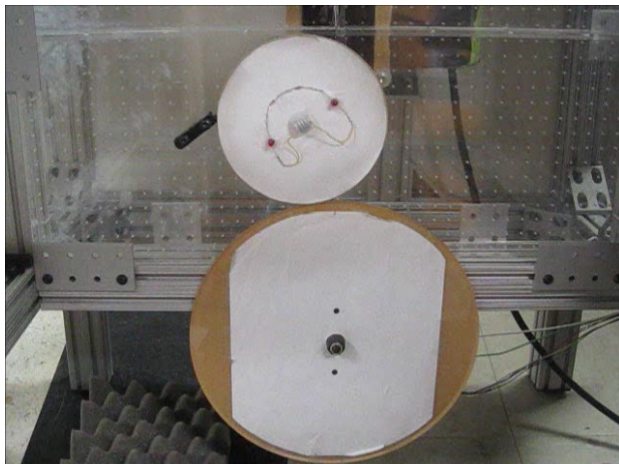
rolling and
balancing

dung beetle
(Nat'l Geo)

bat juggling



vibratory feeding (Sony)



Why Nonprehensile Manipulation?

After all, grasp and carry is “easy” (once a grasp is established); decouples grasp planning and kinematic motion planning.

Why Nonprehensile Manipulation?

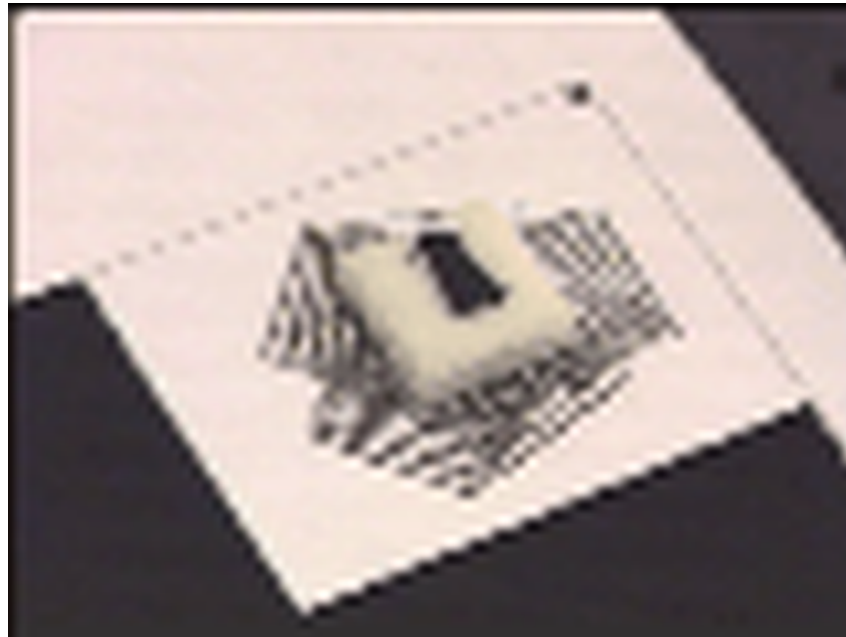
- Manipulate objects too large or heavy to be grasped
- Manipulate several objects simultaneously
- Given a task, use cheaper, lower-DOF robots (automation)
- Given a robot, increase the set of solvable tasks
- Most manipulation is nonprehensile!

Research Topics

- sensing/observability/uncertainty
- contact modeling and mechanics
- motion planning
- feedback control
- understanding what tasks are solvable (e.g., reachable sets, controllability)

Carnegie Mellon, ca. 1994

mechanics, controllability, and planning for pushing

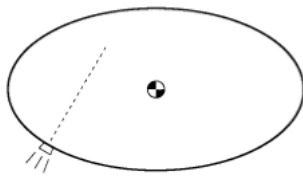


Controllability of a Rigid Body through Unilateral Contact

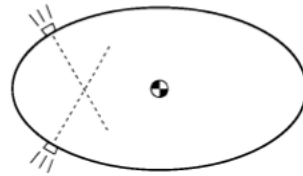
IEEE TRANSACTIONS ON AUTOMATIC CONTROL, VOL. 44, NO. 6, JUNE 1999

Controllability of a Planar Body with Unilateral Thrusters

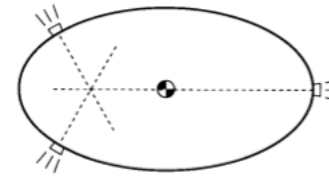
Kevin M. Lynch



accessible



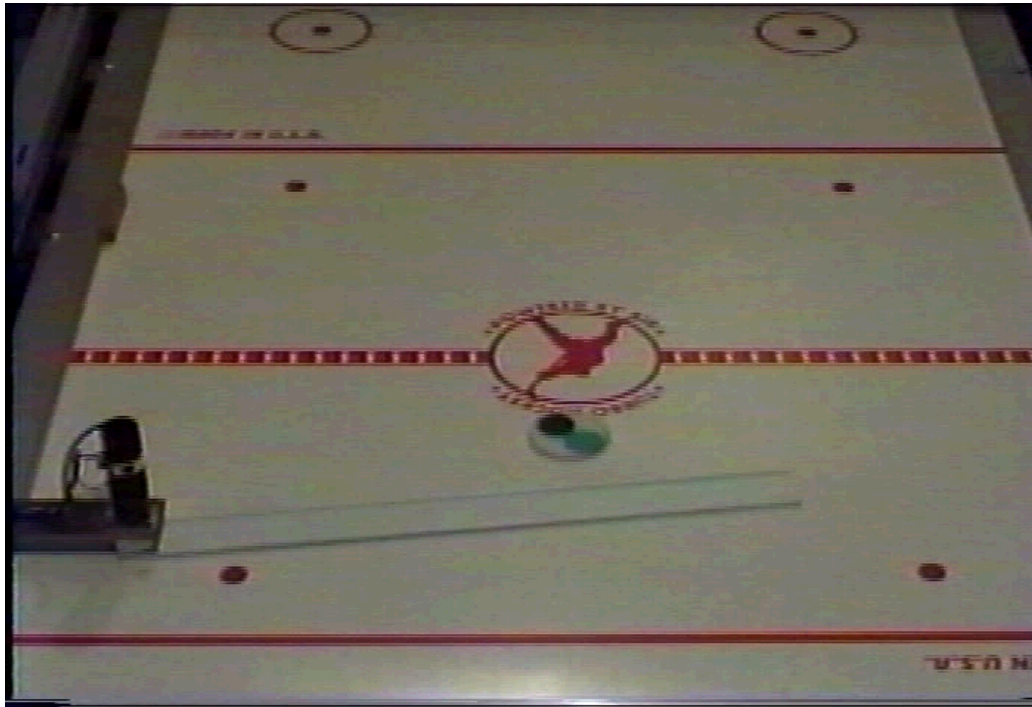
globally controllable



STLC

Northwestern, ca. 1998

feedback stabilization of control-recurrent systems
“juggling”



Controllability of a Rigid Body through Unilateral Contact



Systems & Control Letters 42 (2001) 333–345



www.elsevier.com/locate/sysconle

Impact controllability of an air hockey puck[☆]

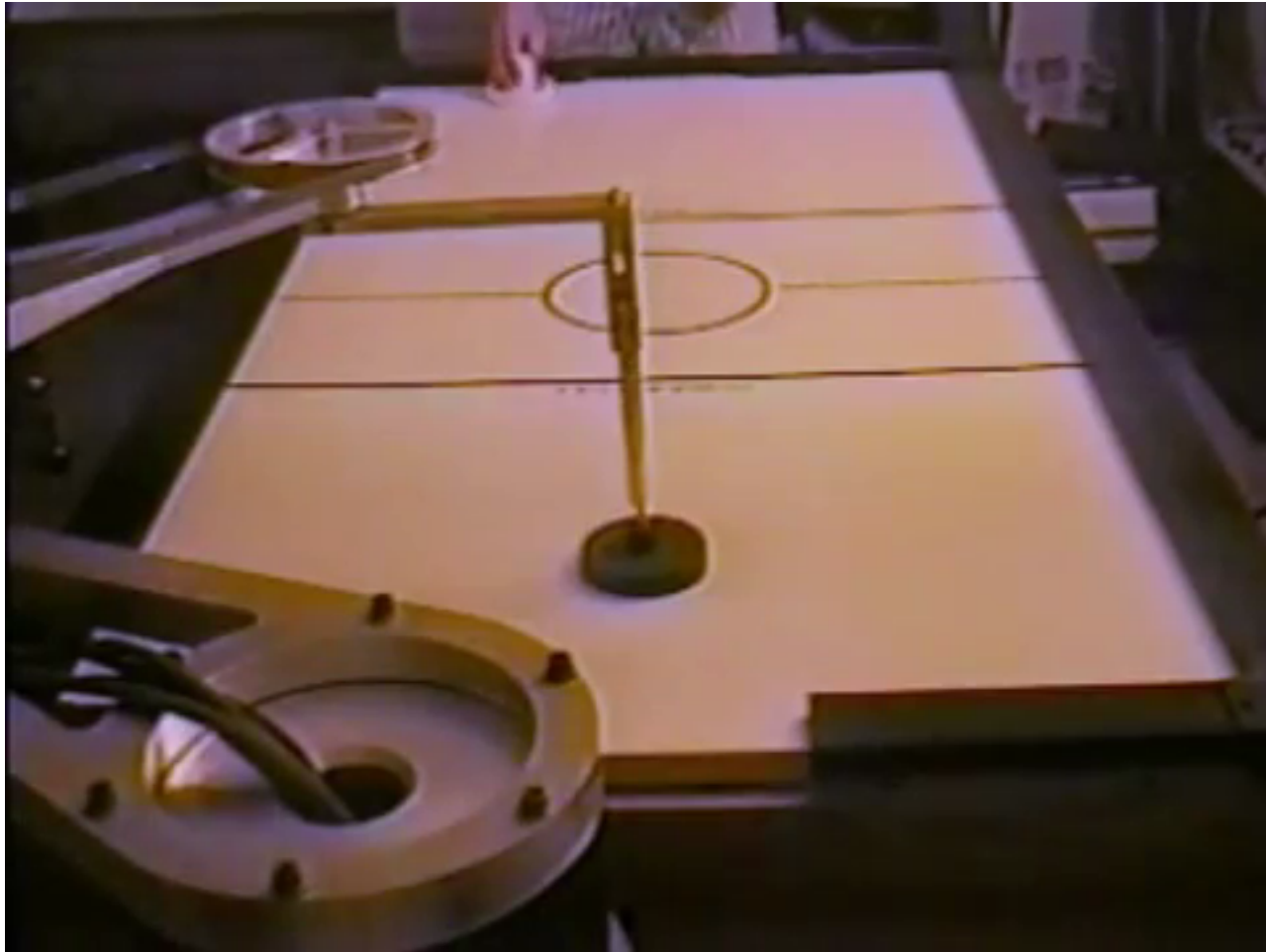
Mark W. Spong^{*}

Coordinated Science Laboratory, University of Illinois at Urbana-Champaign, 1308 W. Main Street, Urbana, IL 61801, USA

Received 15 April 2000; received in revised form 19 October 2000

UIUC, ca. 1999

Bishop and Spong



a few nice things Mark's done for me

- research inspiration
- invited me to my first Allerton conference
- hooked me up with Francesco
- my first trip to Mexico City, CCA 2001
- letters (tenure, IEEE Fellow, etc.)

a few nice things Mark's done for me

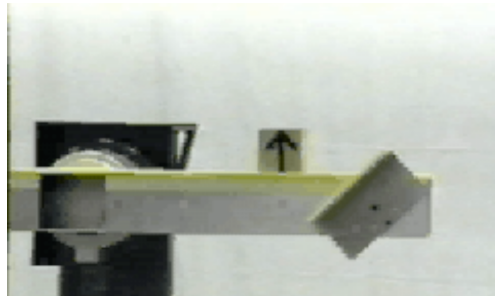
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- sent Bobby Gregg my way!

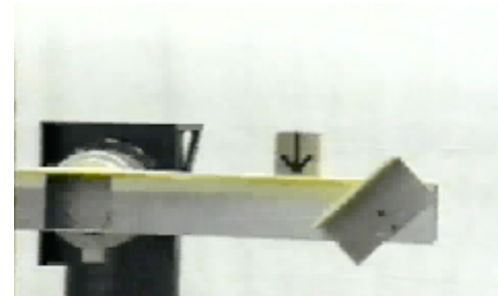


Carnegie Mellon, ca. 1995

underactuated hybrid dynamic manipulation
one actuator, three part DOF

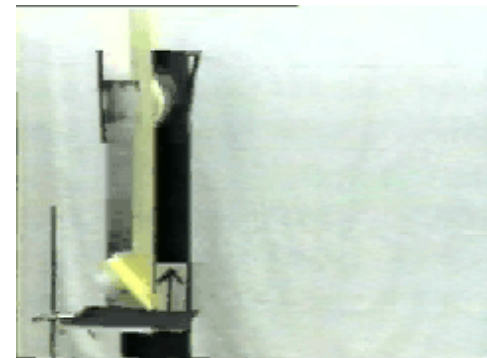
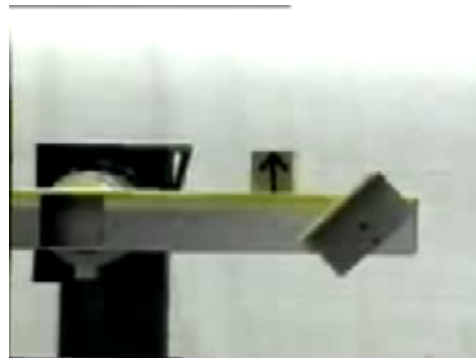
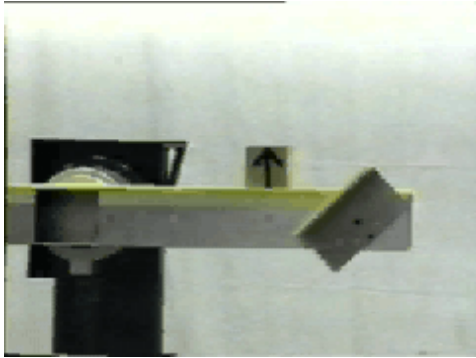


start



goal

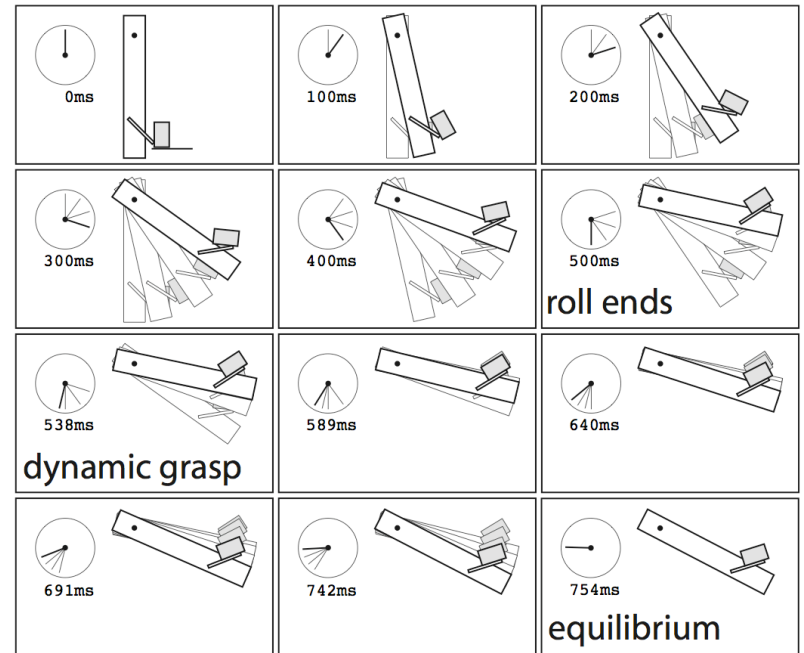
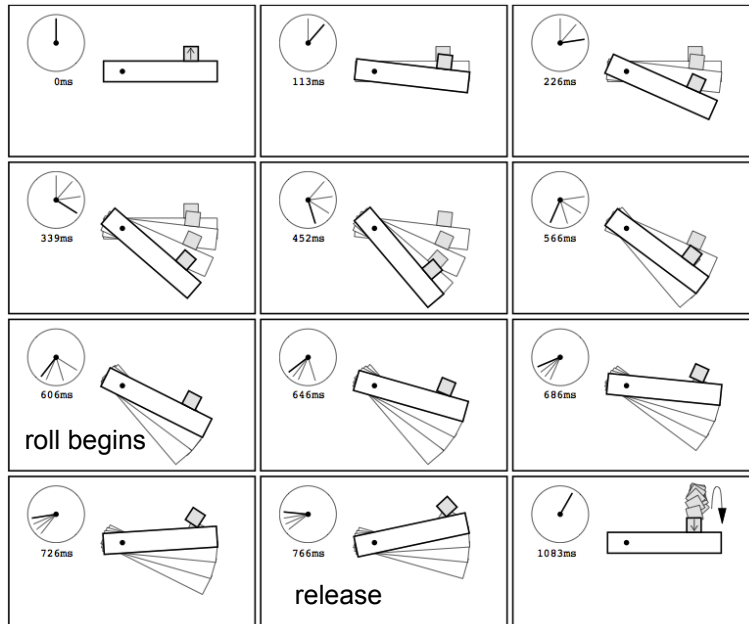
Underactuated Hybrid Manipulation



“grasp” + roll + free flight

¼ speed

roll + “grasp” + free flight



Sequencing Primitives

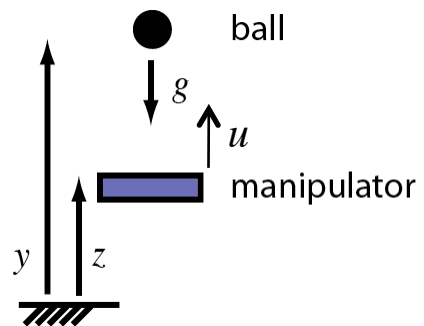
Manipulation consists of a sequence of primitives:

- grasping
- rolling
- manipulator transit motions (no contact)
- pushing
- pivoting
- toppling
- caging
- etc.

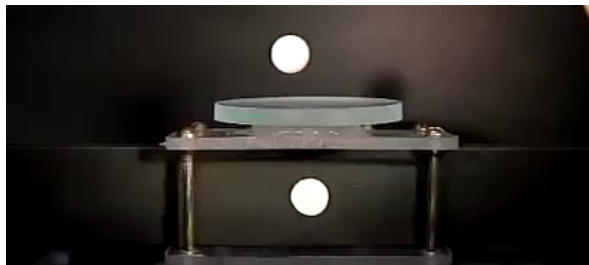
Each primitive is described by different contacts and equations of motion.

A sequence of primitives defines a *hybrid system*.

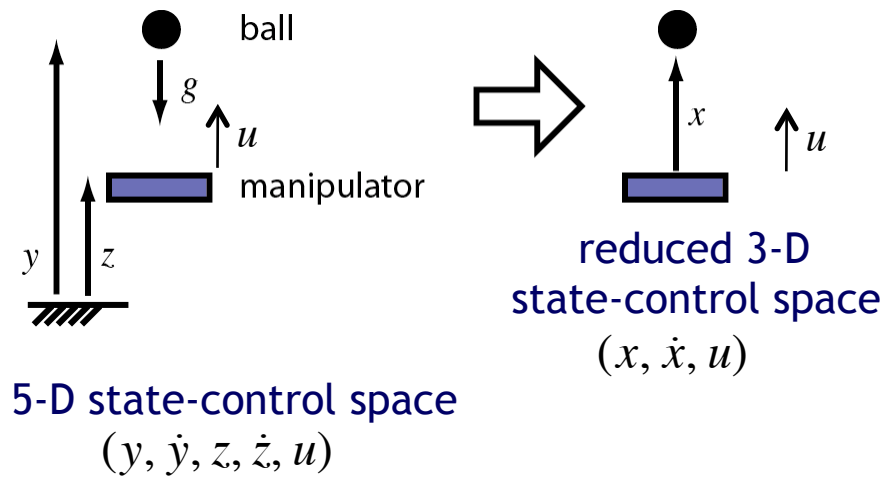
Manipulation as a Hybrid System



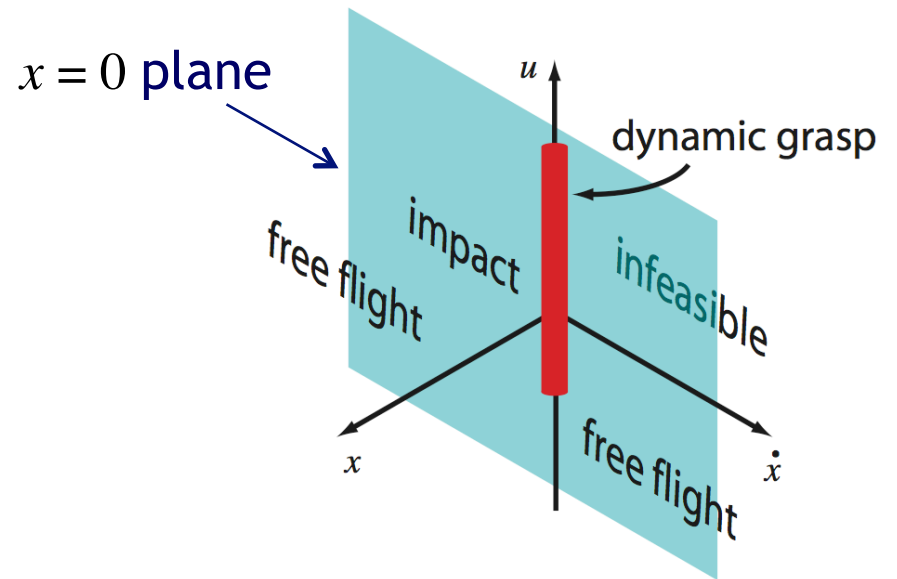
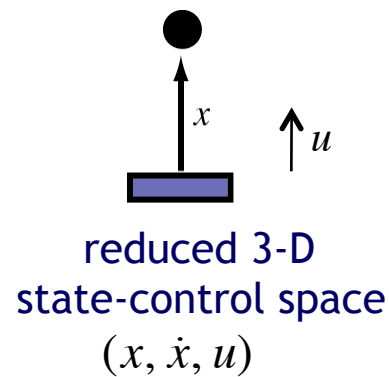
5-D state-control space
 $(y, \dot{y}, z, \dot{z}, u)$



Manipulation as a Hybrid System



Manipulation as a Hybrid System



state-control vector: $w = (x, \dot{x}, u)$

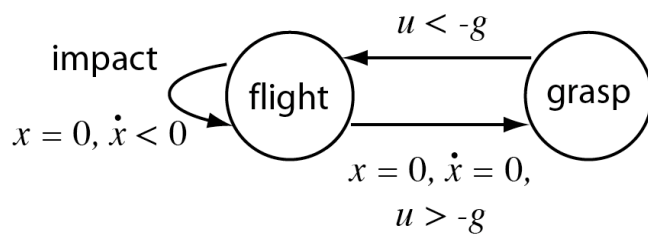
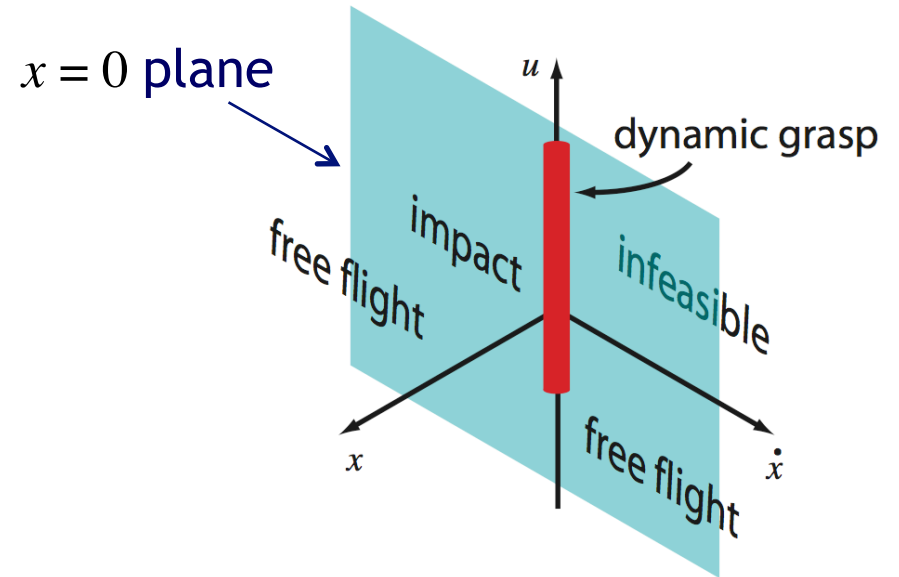
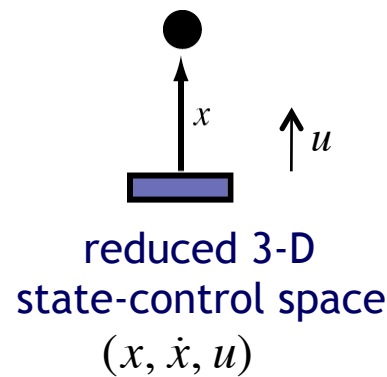
infeasible: $\{w : x < 0\}$

impact: $\{w : x = 0, \dot{x} < 0\}$

“dynamic grasp”: $\{w : x = 0, \dot{x} = 0, u > -g\}$

free flight: remaining w

Manipulation as a Hybrid System



graph representing the
topology of the hybrid system

state-control vector: $w = (x, \dot{x}, u)$

infeasible: $\{w : x < 0\}$

impact: $\{w : x = 0, \dot{x} < 0\}$

“dynamic grasp”: $\{w : x = 0, \dot{x} = 0, u > -g\}$

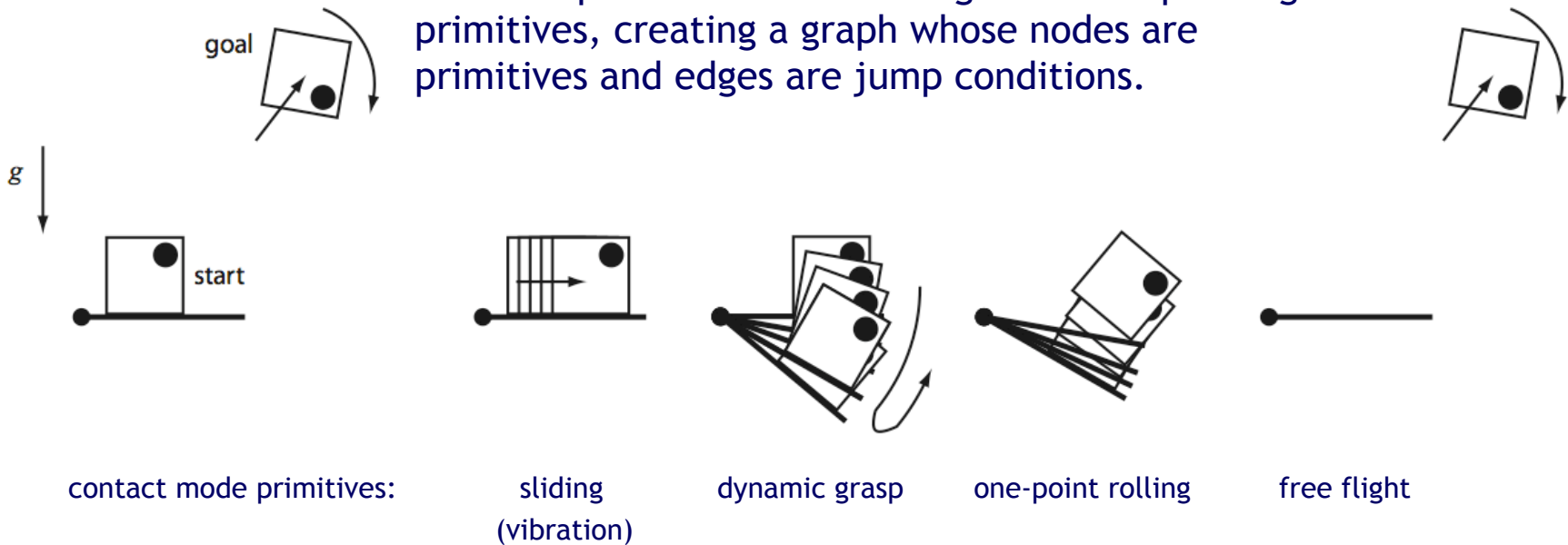
free flight: remaining w

Hybrid Sequence Planning

- 3 part positions
 - + 3 part velocities
 - + 1 arm position
 - + 1 arm velocity
 - + 1 arm control
-

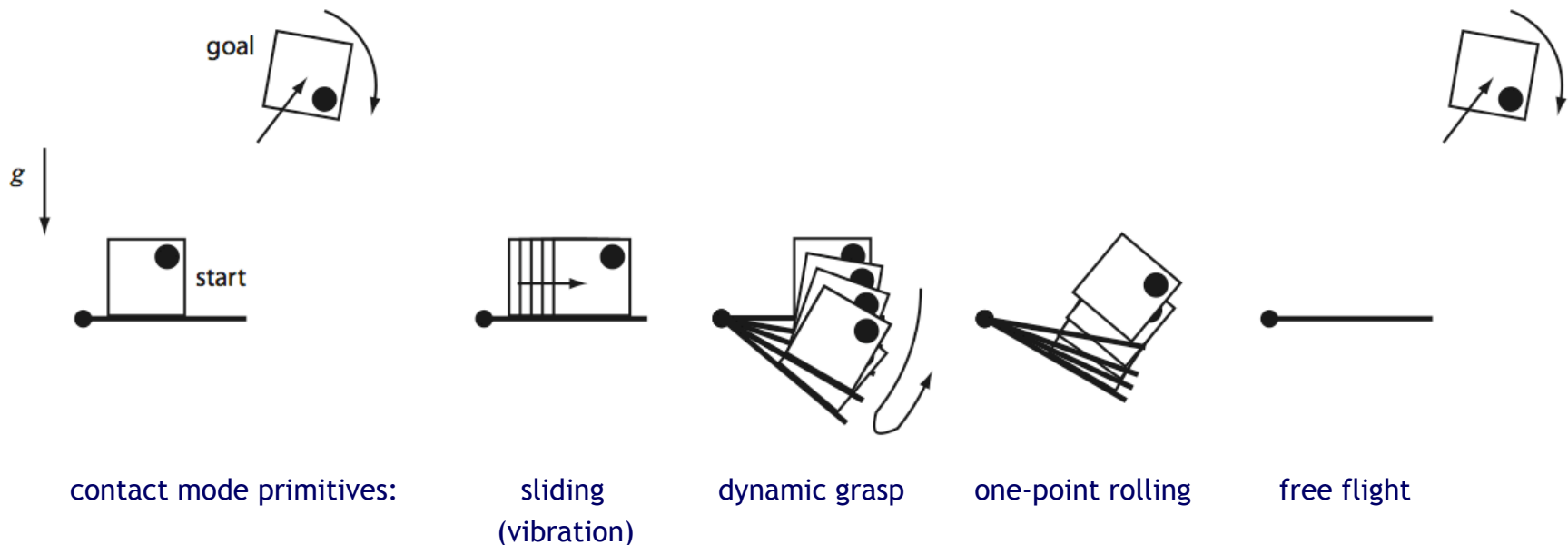
9-dimensional state-control space

The 9-D space is carved into regions corresponding to primitives, creating a graph whose nodes are primitives and edges are jump conditions.



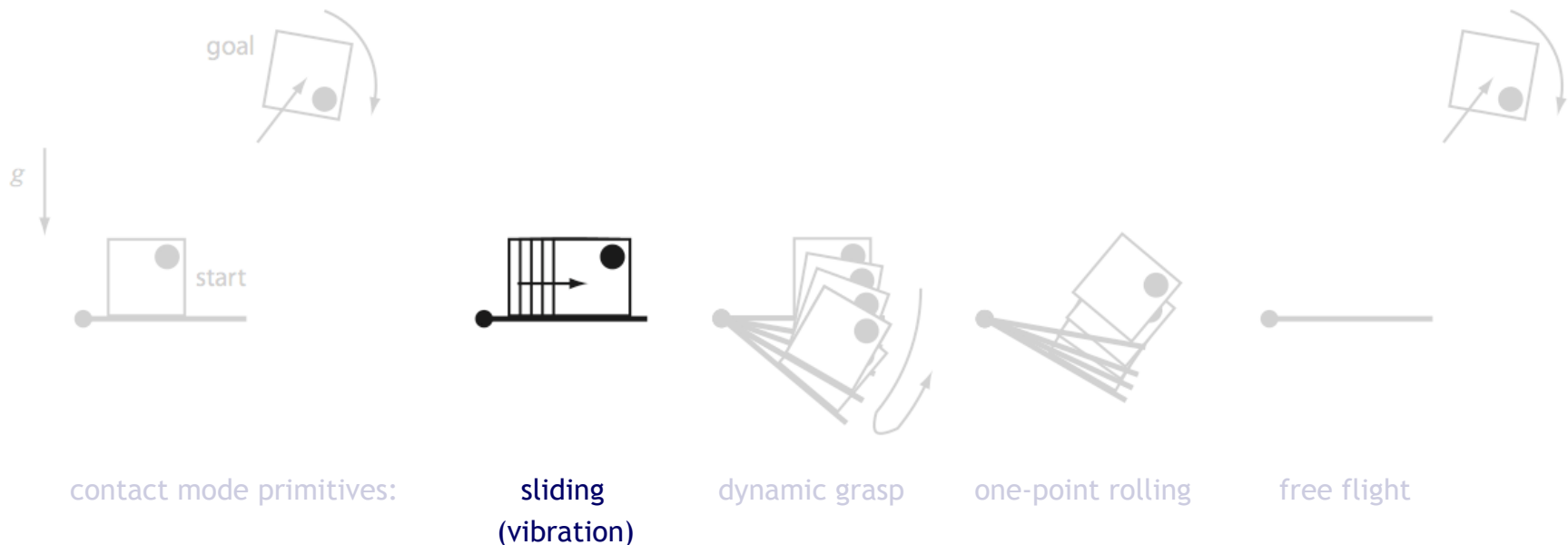
Hybrid Sequence Planning

1. Choose a sequence of primitives and find the state-control jump conditions between them. Jumps occur at contact transitions (established/broken, sticking/sliding).
2. Find controls within each primitive between jump conditions.



Hybrid Sequence Planning

1. Choose a sequence of primitives and find the state-control jump conditions between them. Jumps occur at contact transitions (established/broken, sticking/sliding).
2. Find controls within each primitive between jump conditions.



Some Simpsons-Inspired Research



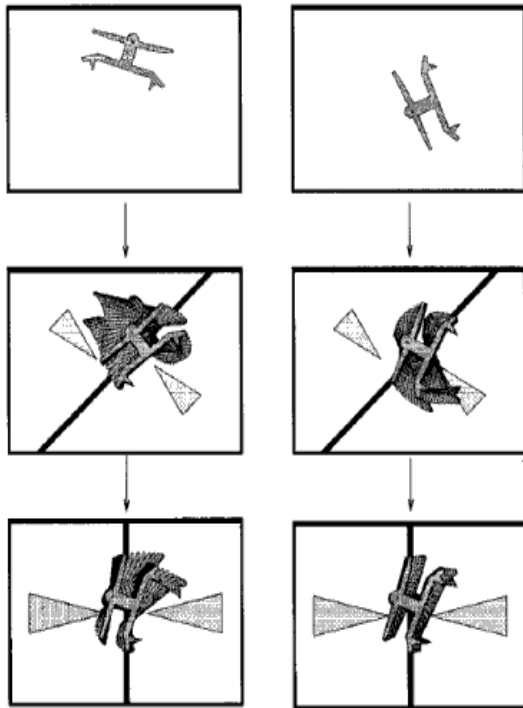
More Simpsons-Inspired Research



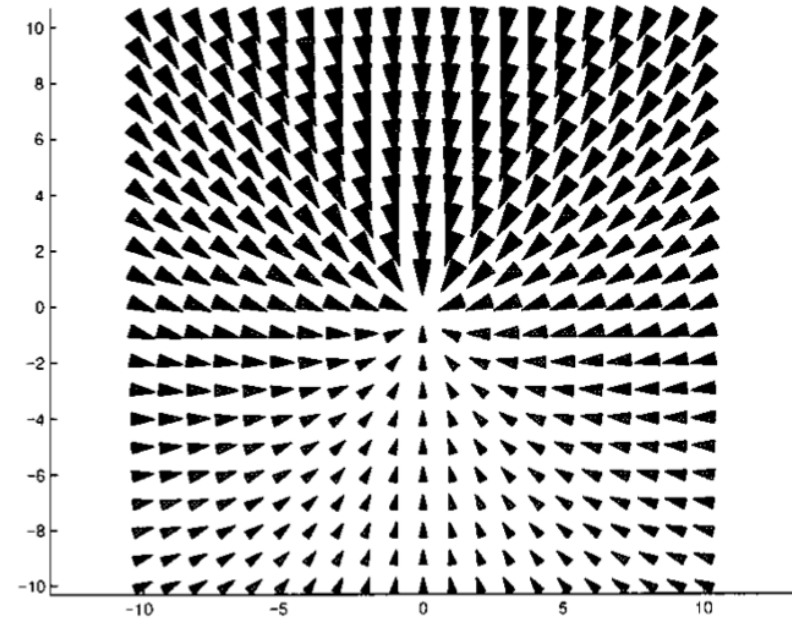
More Simpsons-Inspired Research



Programmable Motion Surfaces



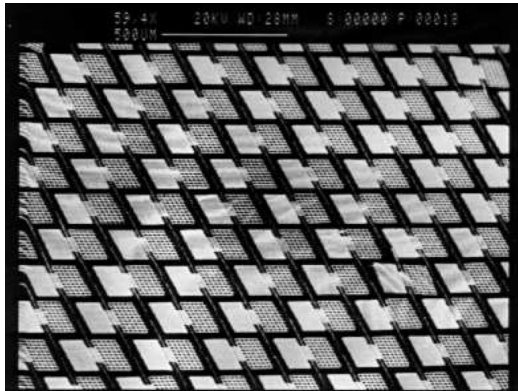
a sequence of force fields
for sensorless orienting



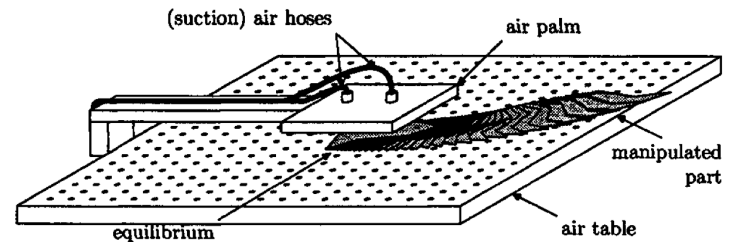
a force field for single-step
positioning and orienting

Bohringer, Donald, MacDonald, Kavraki, Lamiroux, Goldberg

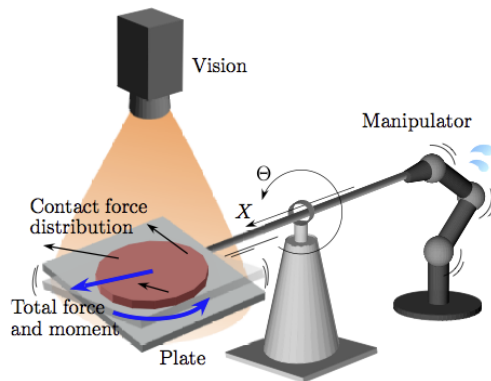
Motion Surface Implementation



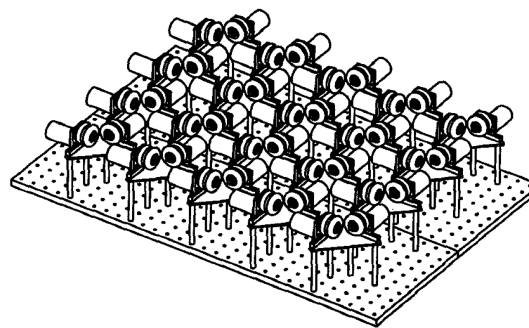
MEMS actuator arrays
Bohringer, Donald, MacDonald



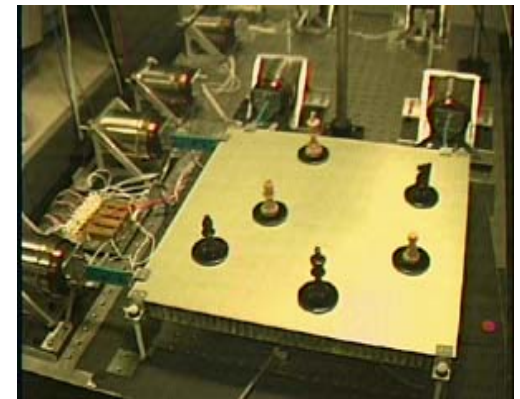
air flow
Luntz, Moon, Laurent



2-DOF pizza manipulation
Higashimori and Kaneko

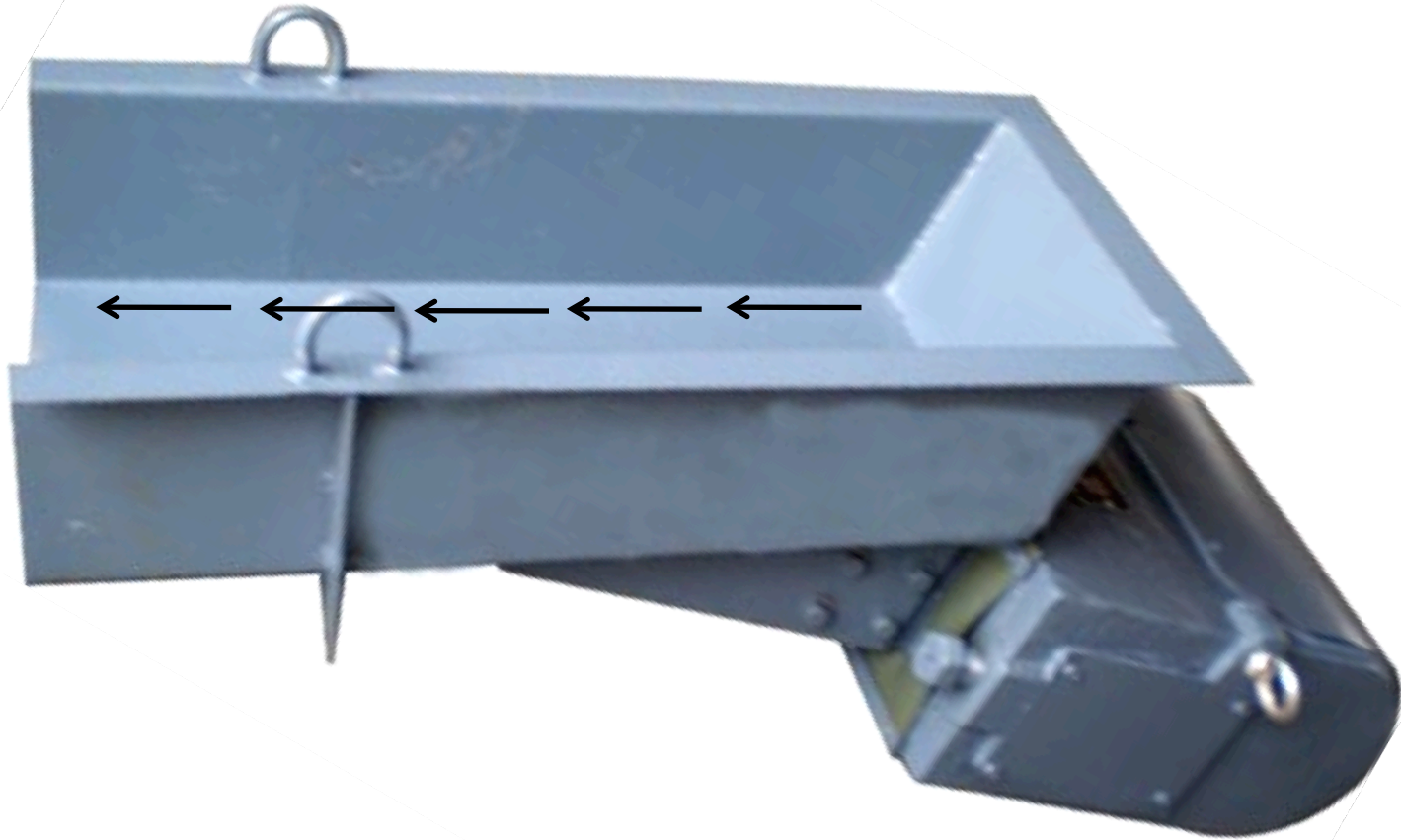


rolling wheels
Luntz, Messner, Choset,
Murphey, Burdick

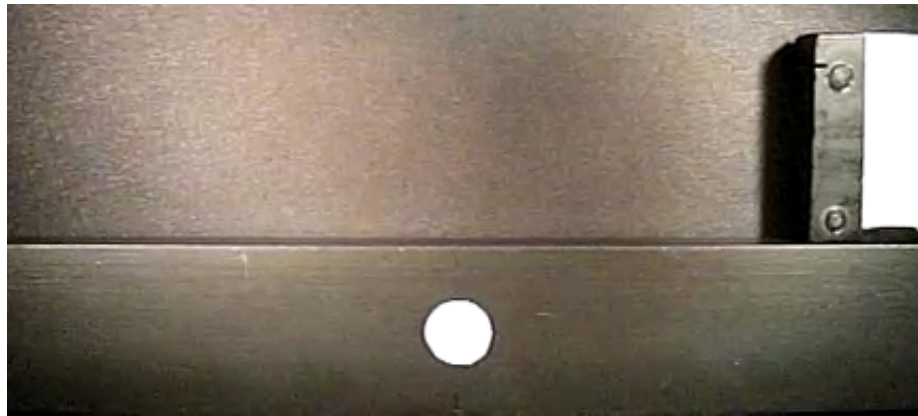


3-DOF horizontally vibrating table
Reznik and Canny

Industrial Vibratory Feeder



Sliding Manipulation

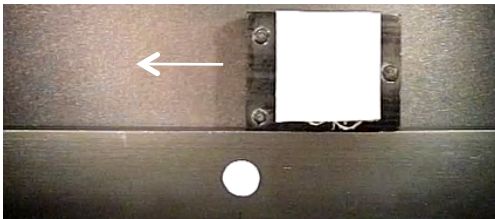


15 Hz vibration
1/20 speed

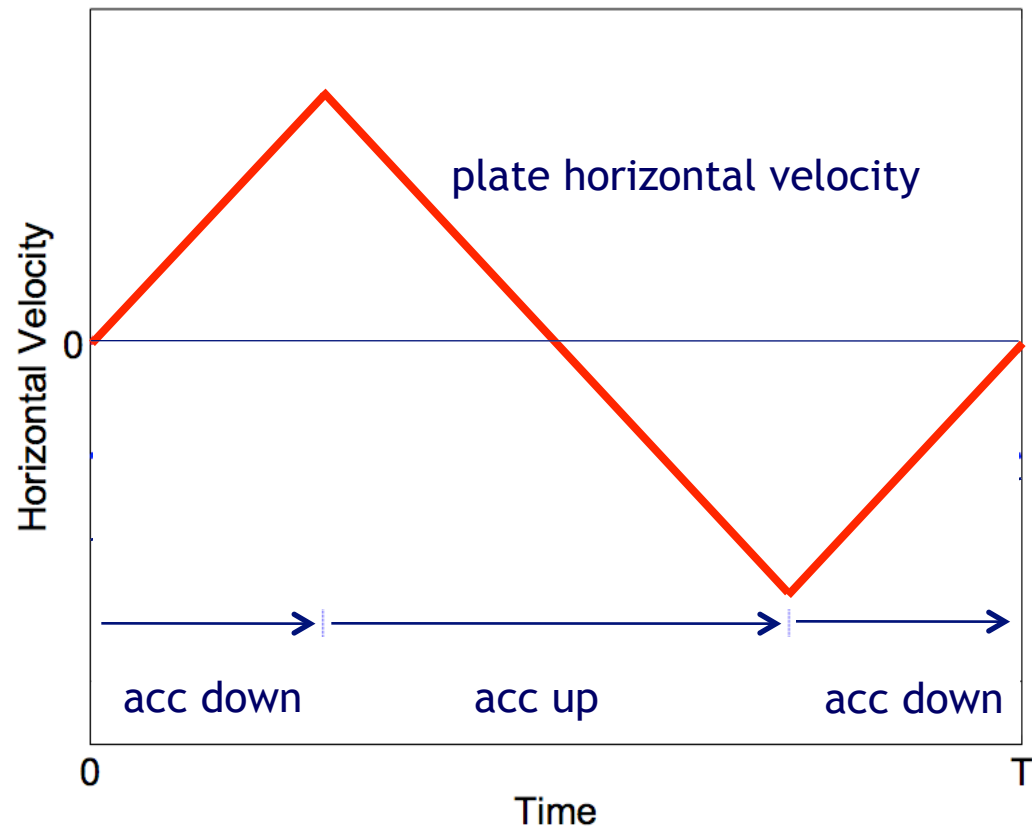
$$f_{\text{fric}} = \mu f_{\text{normal}} \frac{\mathbf{v}_{\text{rel}}}{\|\mathbf{v}_{\text{rel}}\|}$$

Sliding Manipulation

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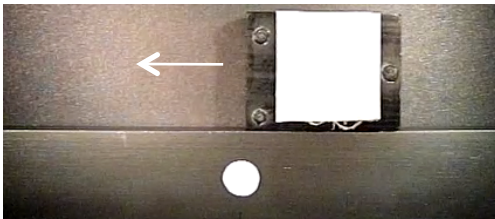


bang-bang vertical and horizontal acceleration

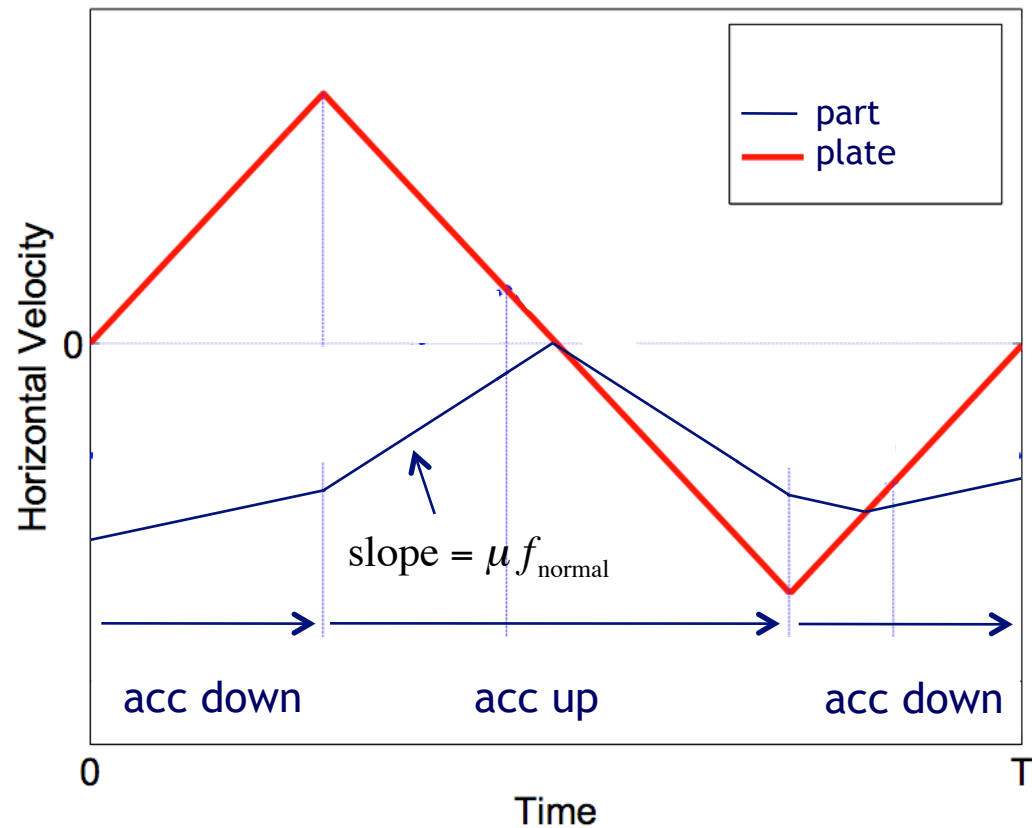


Sliding Manipulation

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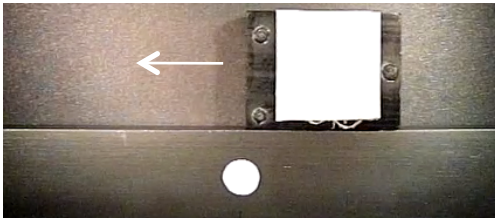


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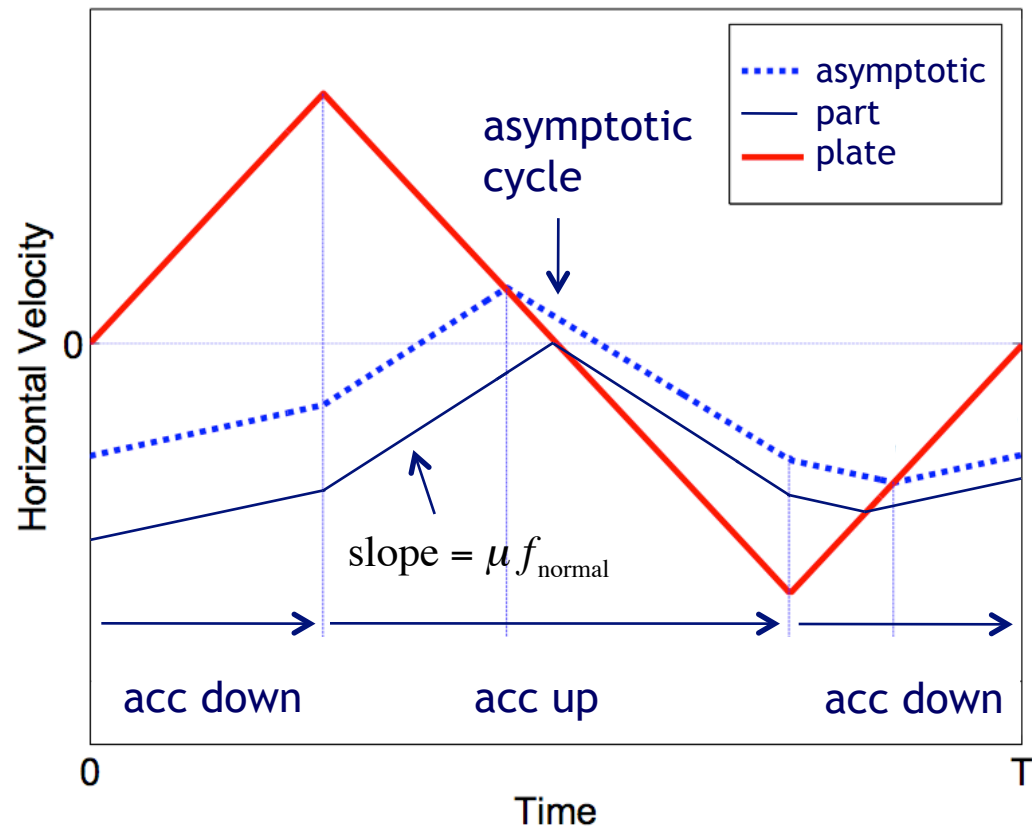


Sliding Manipulation

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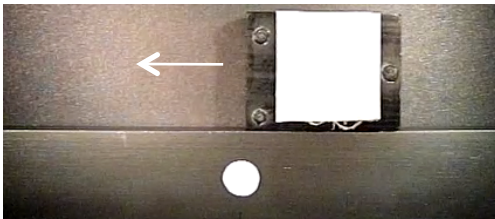


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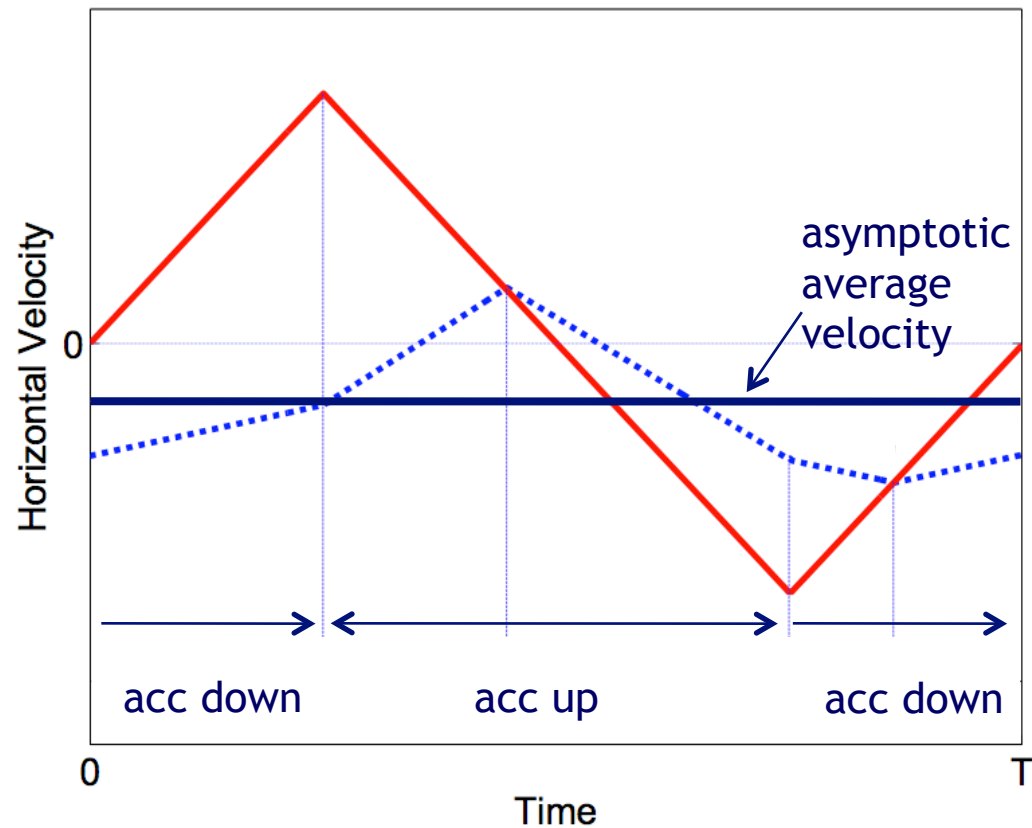


Sliding Manipulation

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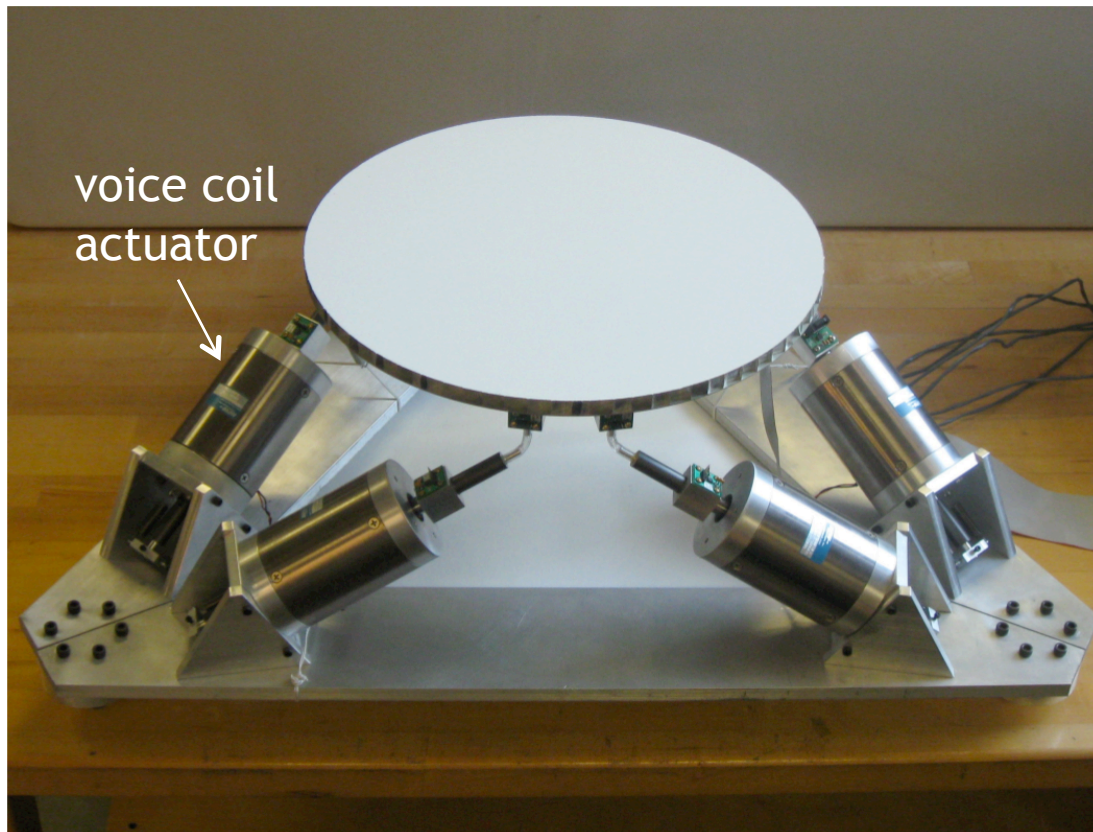


bang-bang vertical and horizontal acceleration



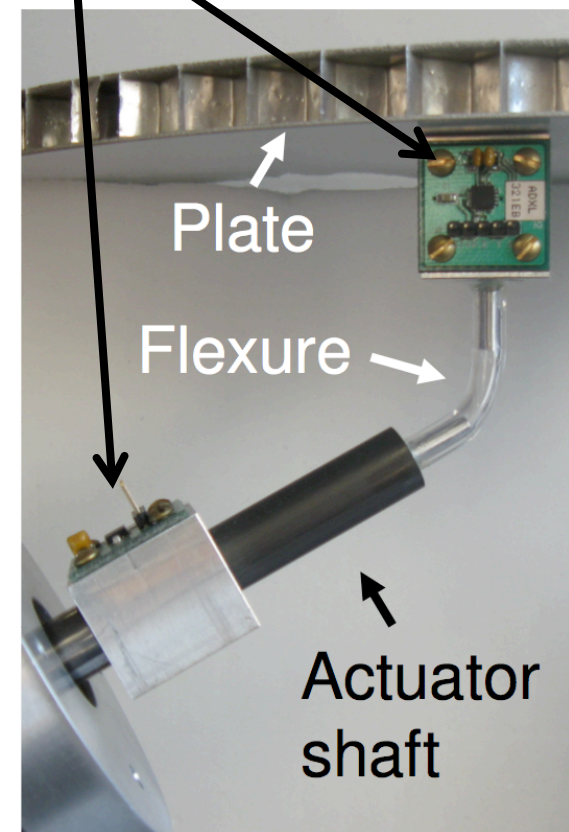
The 6-DOF PPOD

(Programmable Parts Orienting Device)



flexure-based Stewart platform

accelerometers

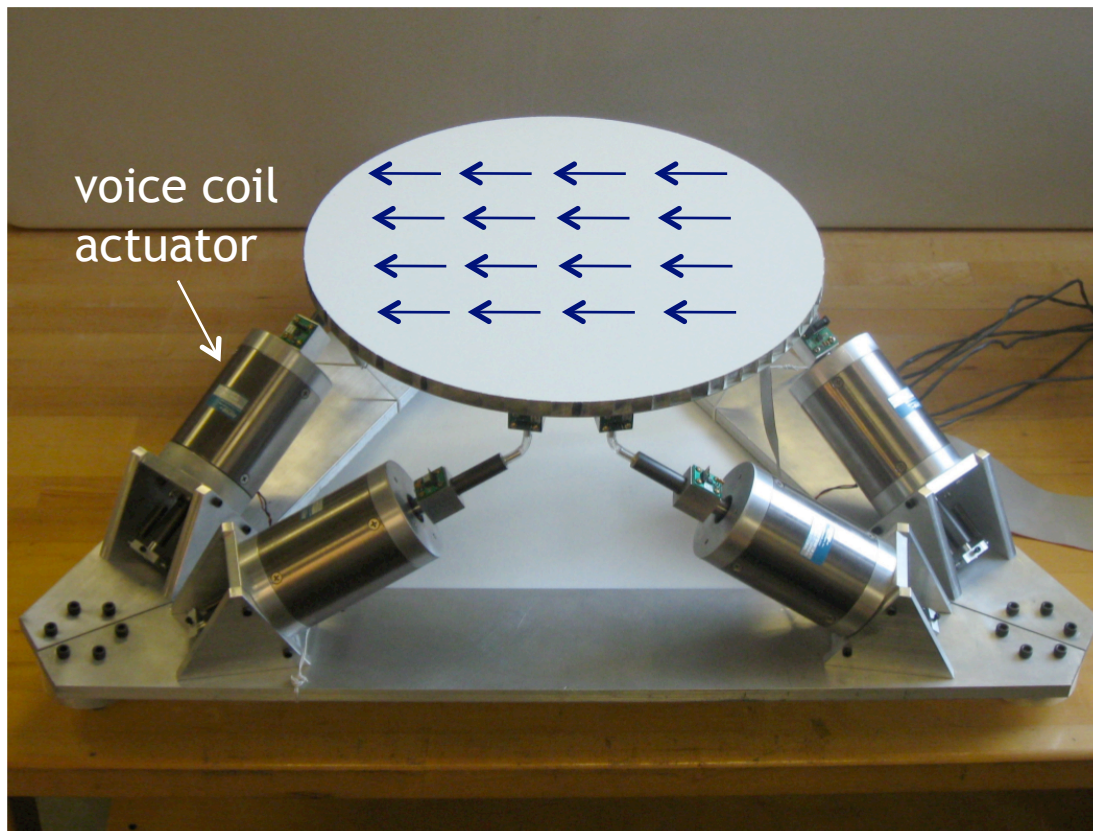


audio
amps



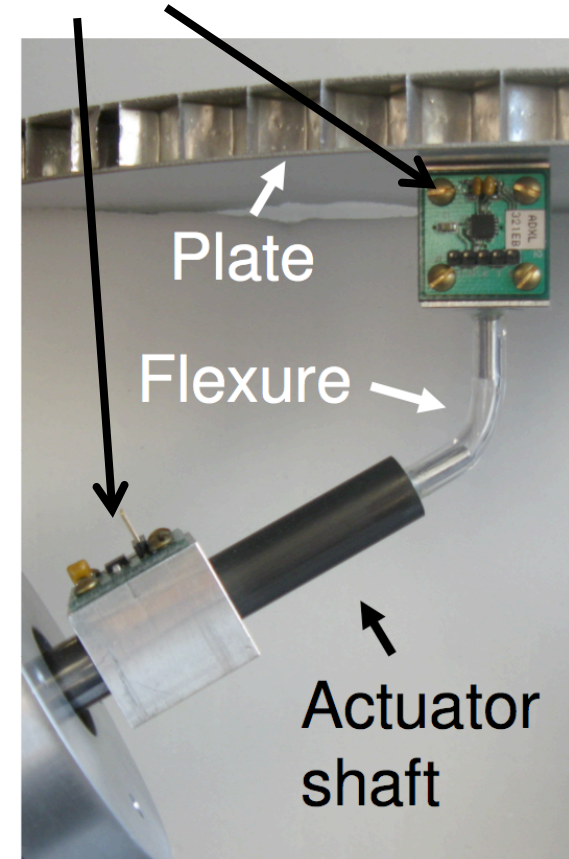
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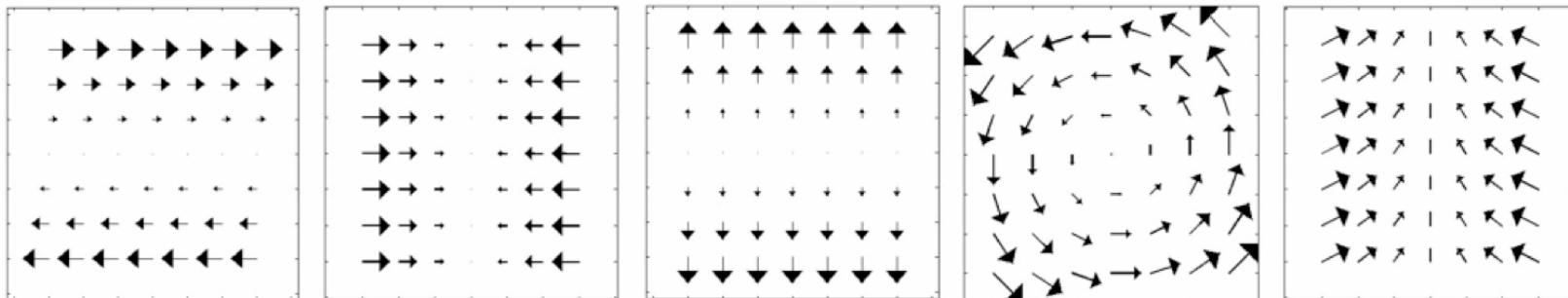
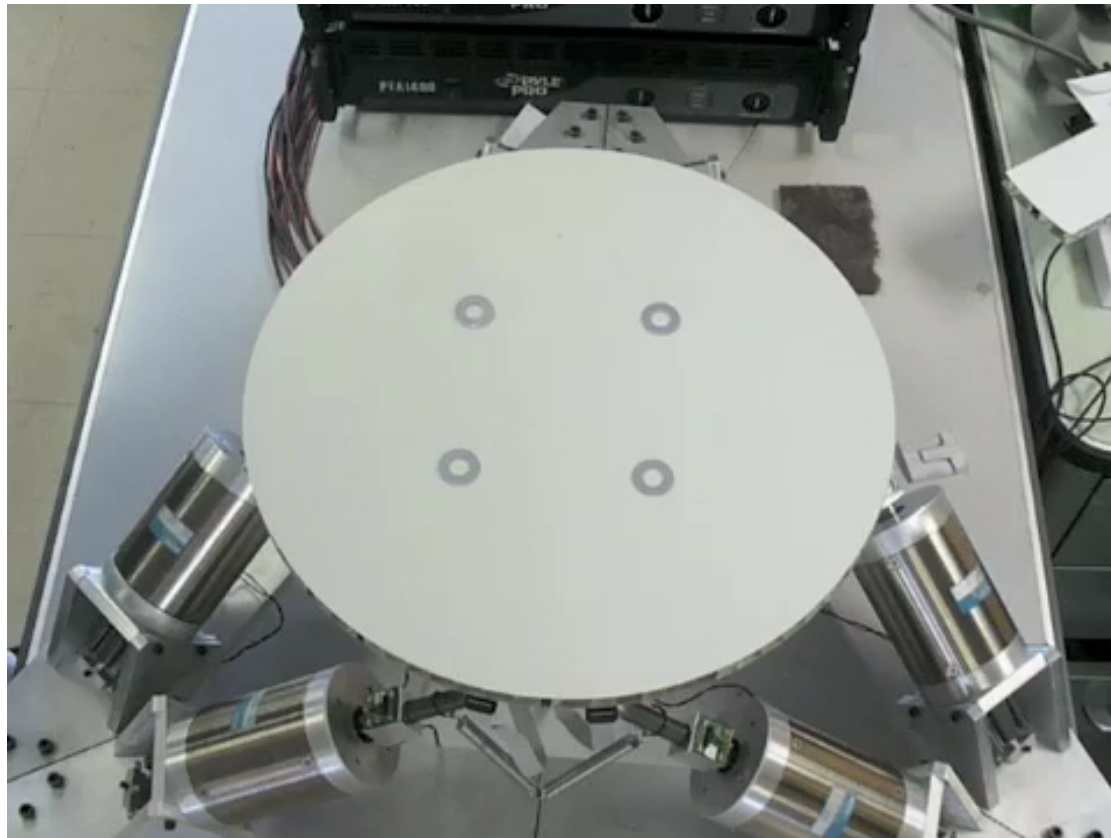


audio
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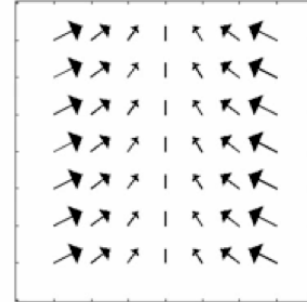
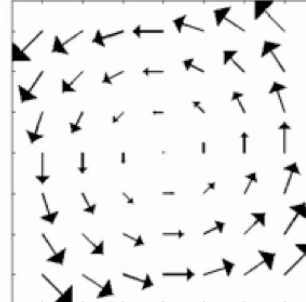
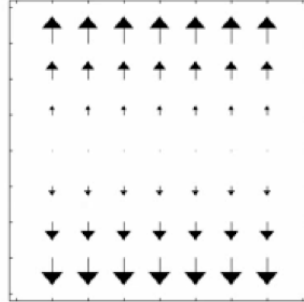
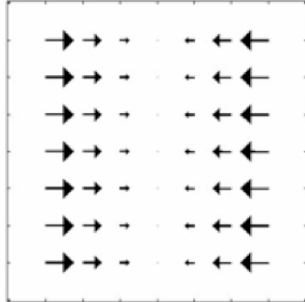
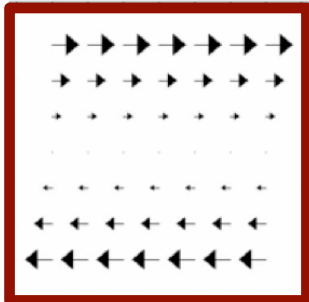
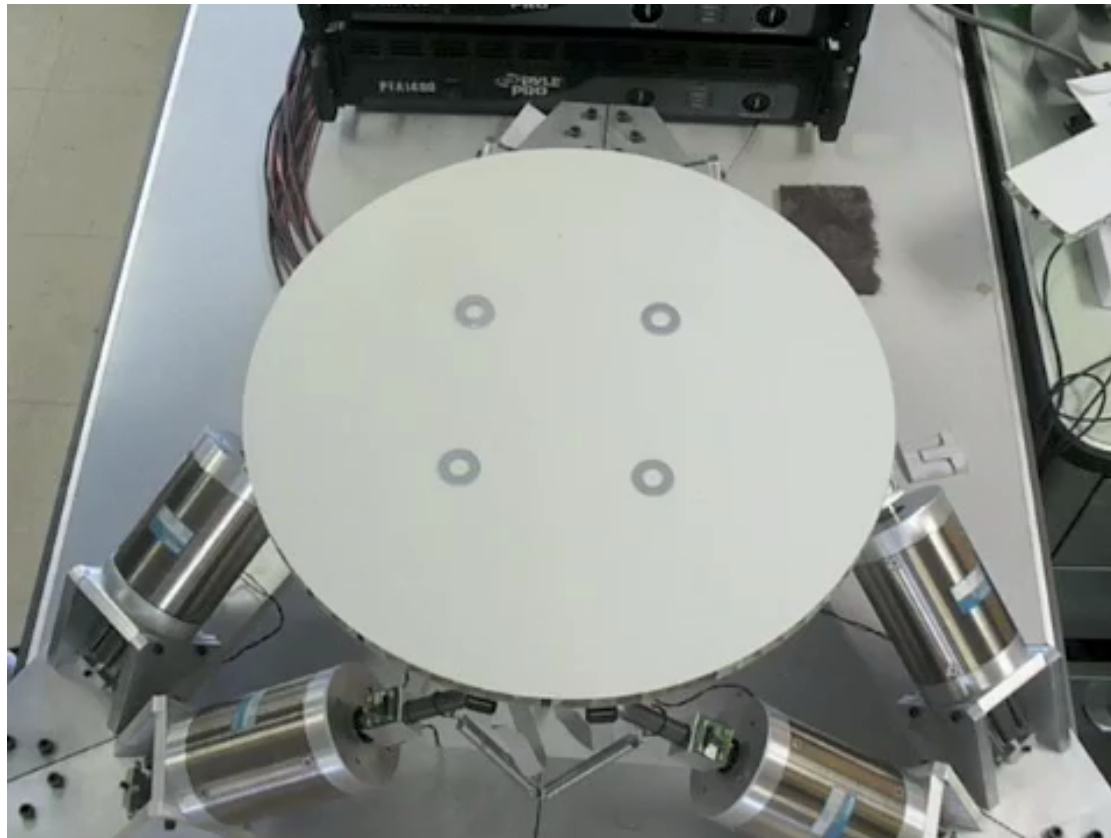
The 6-DOF PPOD

(Programmable Parts Orienting Device)

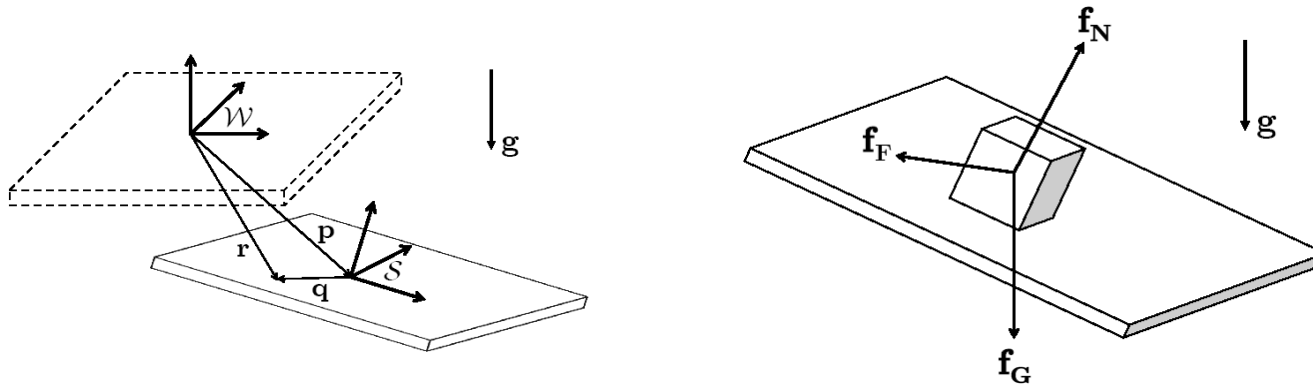


The 6-DOF PPOD

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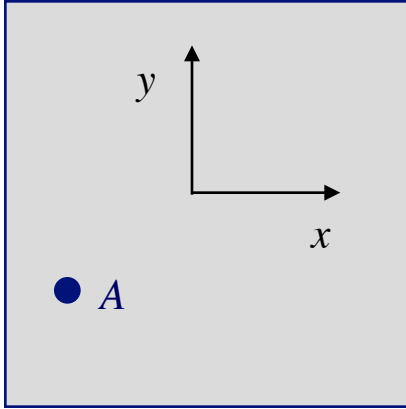
Part Dynamics



$$f_{\text{fric}} = \mu f_{\text{normal}} \frac{\mathbf{V}_{\text{rel}}}{\|\mathbf{V}_{\text{rel}}\|}$$

- $\dot{p}_x, \dot{p}_y, \omega_z$: horizontal velocity determines friction force **direction**
- $\ddot{p}_z, \alpha_x, \alpha_y$: vertical acceleration determines friction force **magnitude**
- 6-DOF motion allows **position-dependent** fields with **nonzero divergence**

Asymptotic Behavior



top view of plate (positions)

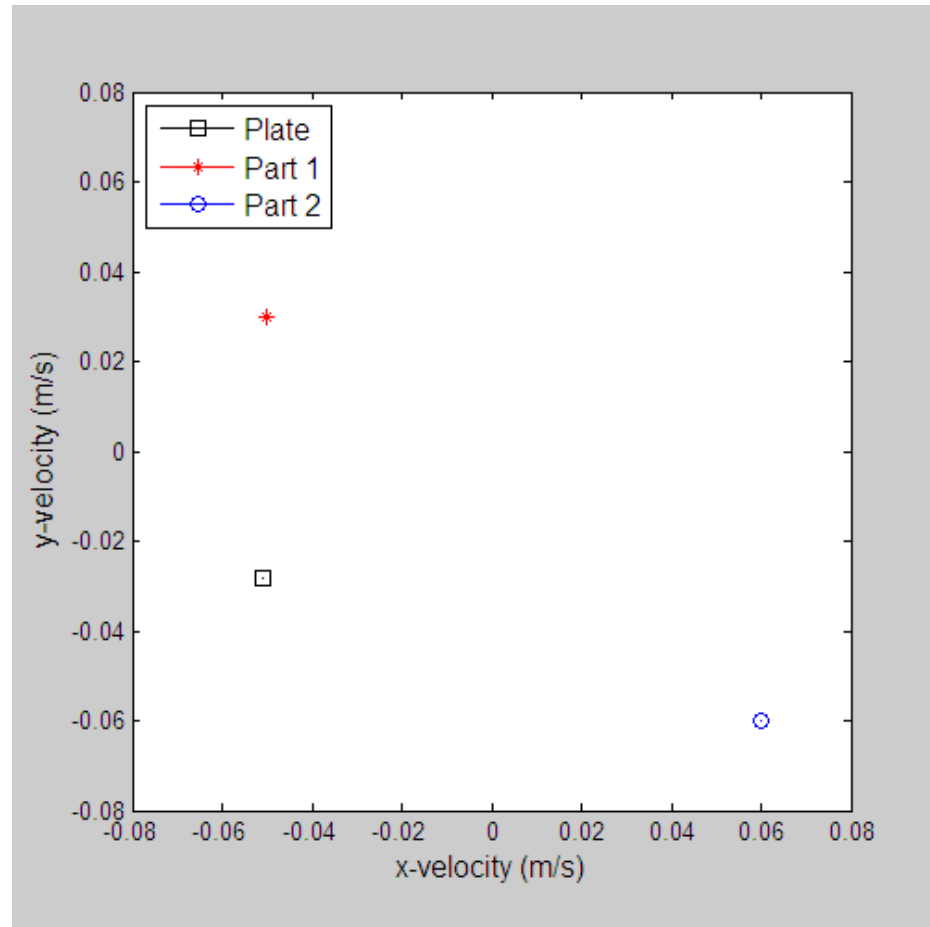
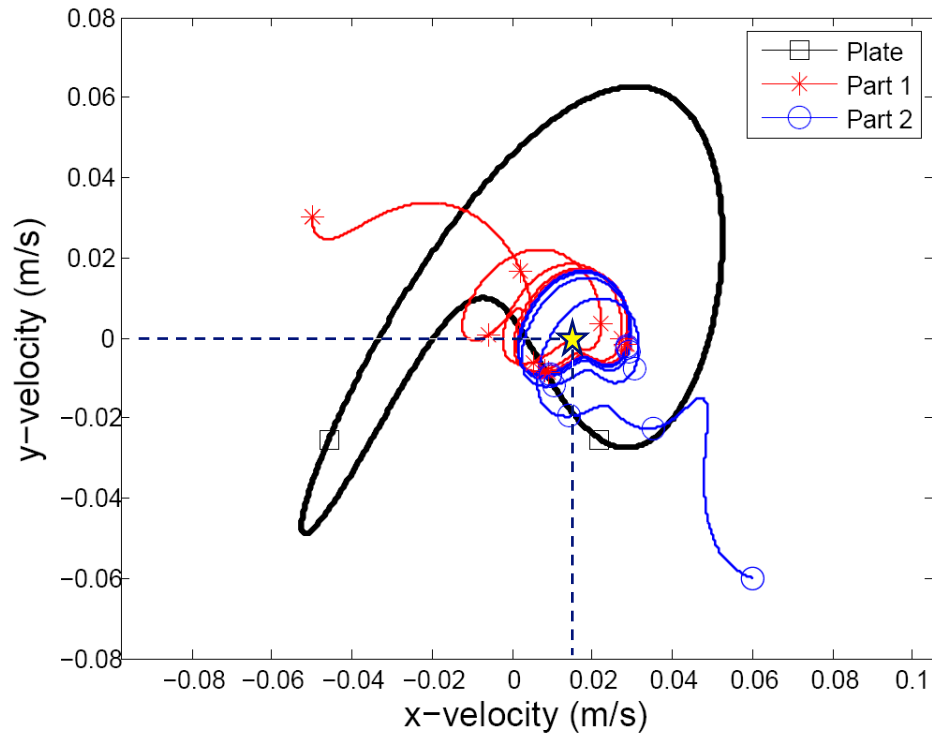


plate and part horizontal velocities at A

$$f_{\text{fric}} = \mu f_{\text{normal}} \frac{\mathbf{v}_{\text{rel}}}{\|\mathbf{v}_{\text{rel}}\|}$$

Asymptotic Velocity

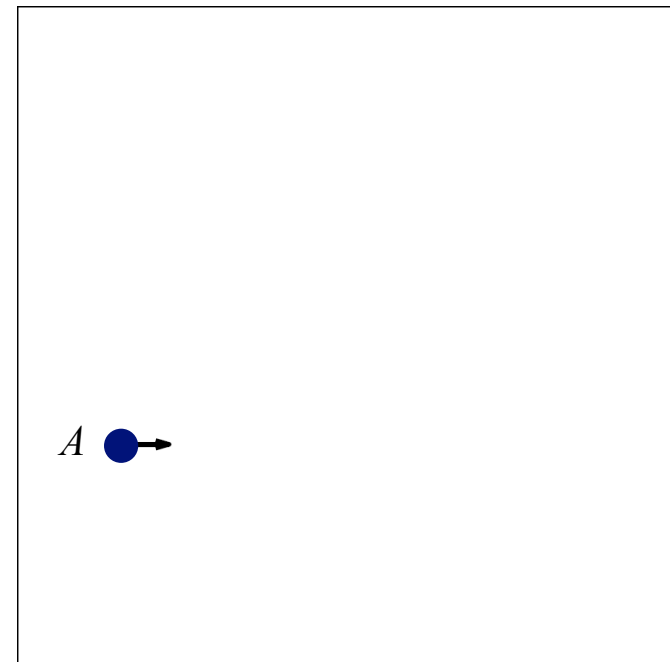
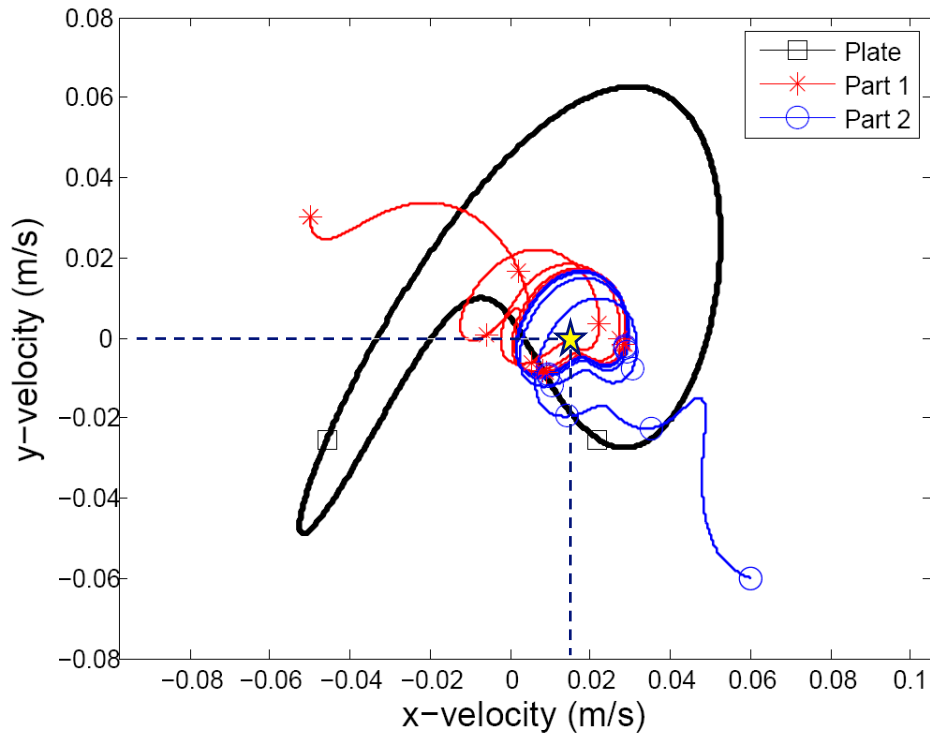


Asymptotic velocity at (x,y) :

$$\mathbf{v}(x, y) = \frac{1}{T} \int_0^T \mathbf{v}'(t) dt$$

where $\mathbf{v}'(t)$ is the limit cycle.

Asymptotic Velocity



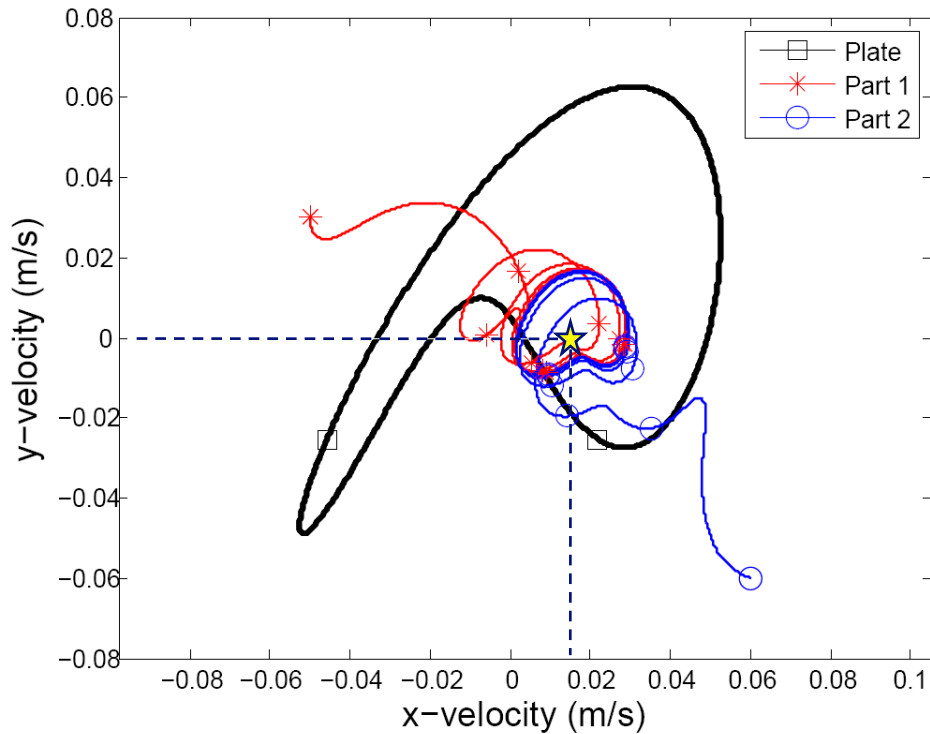
Asymptotic velocity at (x,y) :

$$\mathbf{v}(x,y) = \frac{1}{T} \int_0^T \mathbf{v}'(t) dt$$

where $\mathbf{v}'(t)$ is the limit cycle.

asymptotic velocity vector at A

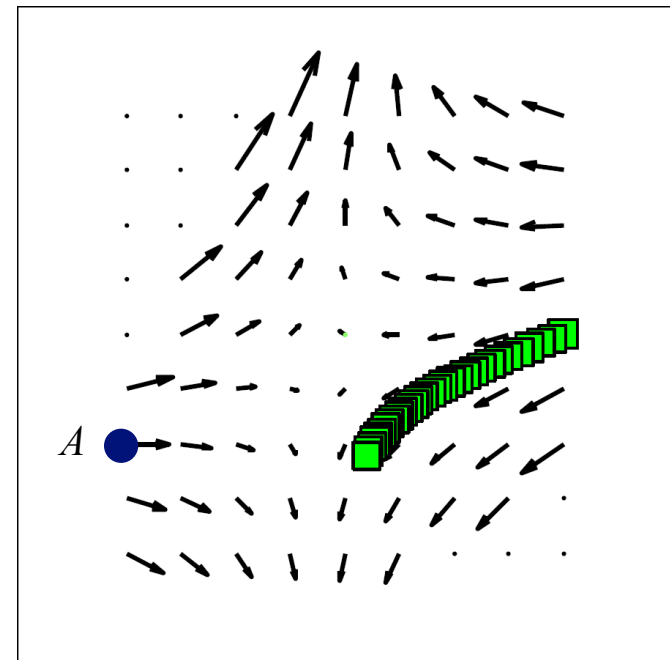
Asymptotic Velocity



Asymptotic velocity at (x,y) :

$$\mathbf{v}(x,y) = \frac{1}{T} \int_0^T \mathbf{v}'(t) dt$$

where $\mathbf{v}'(t)$ is the limit cycle.

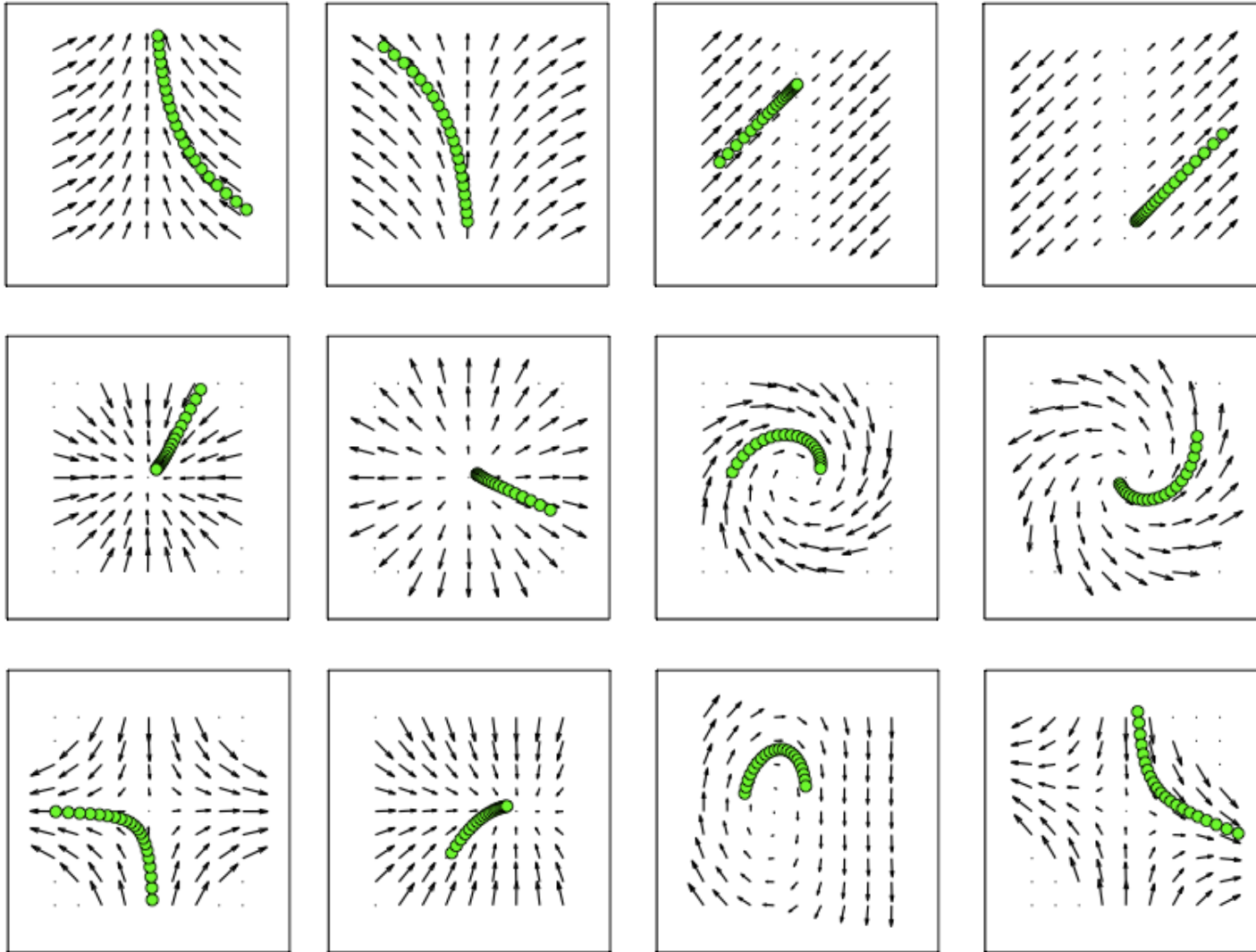


asymptotic velocity vectors at all points:

asymptotic velocity field

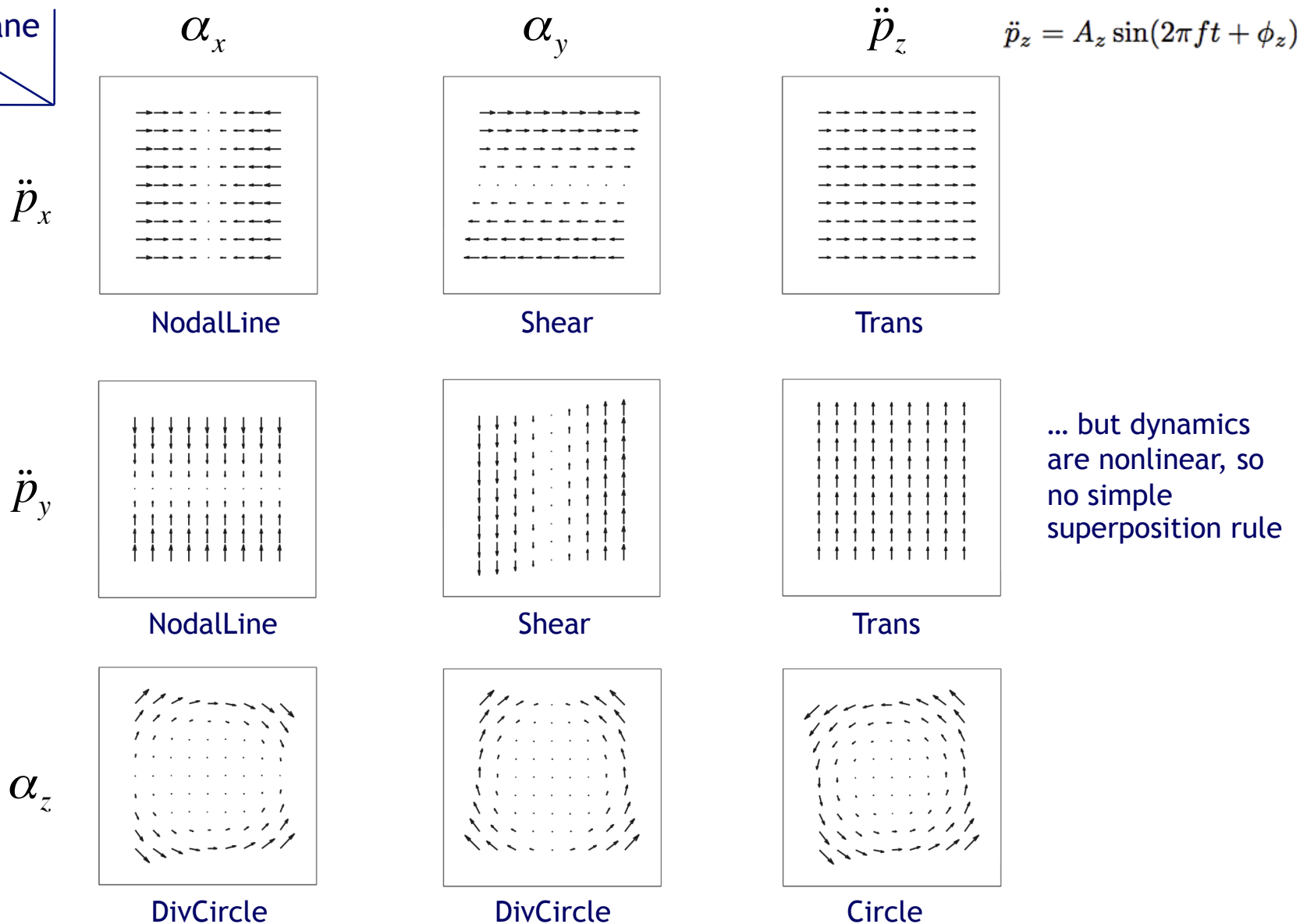
(not a force field)

Which Velocity Fields Are Possible?



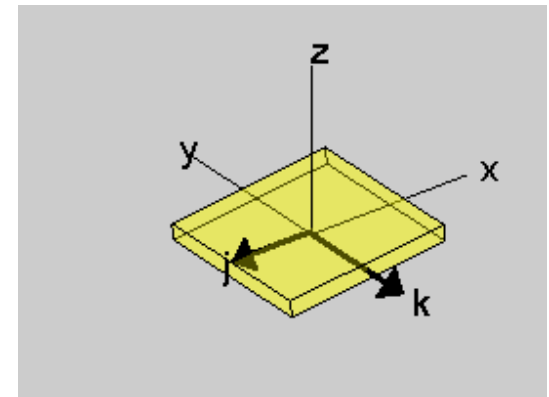
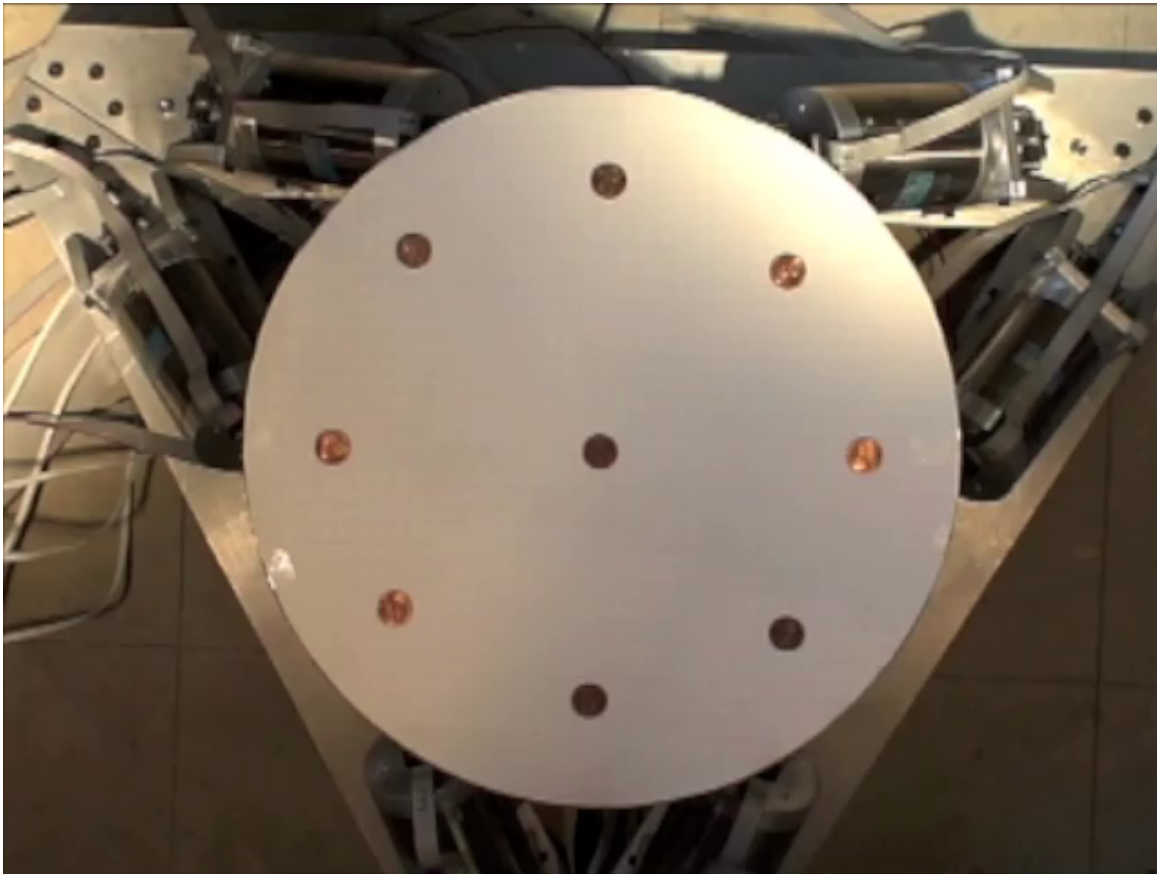
Single Frequency “Basis” Fields

out-of-plane
in-plane

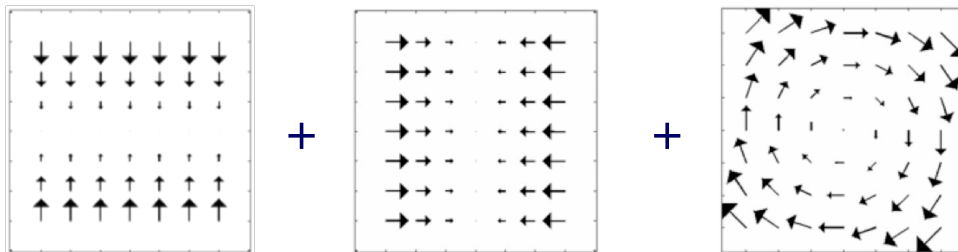
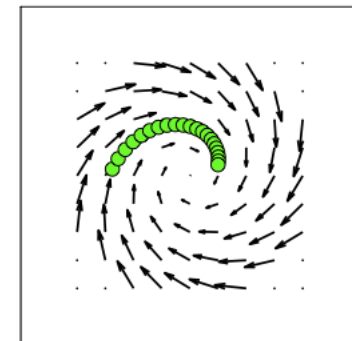


... but dynamics are nonlinear, so no simple superposition rule

Whirlpool



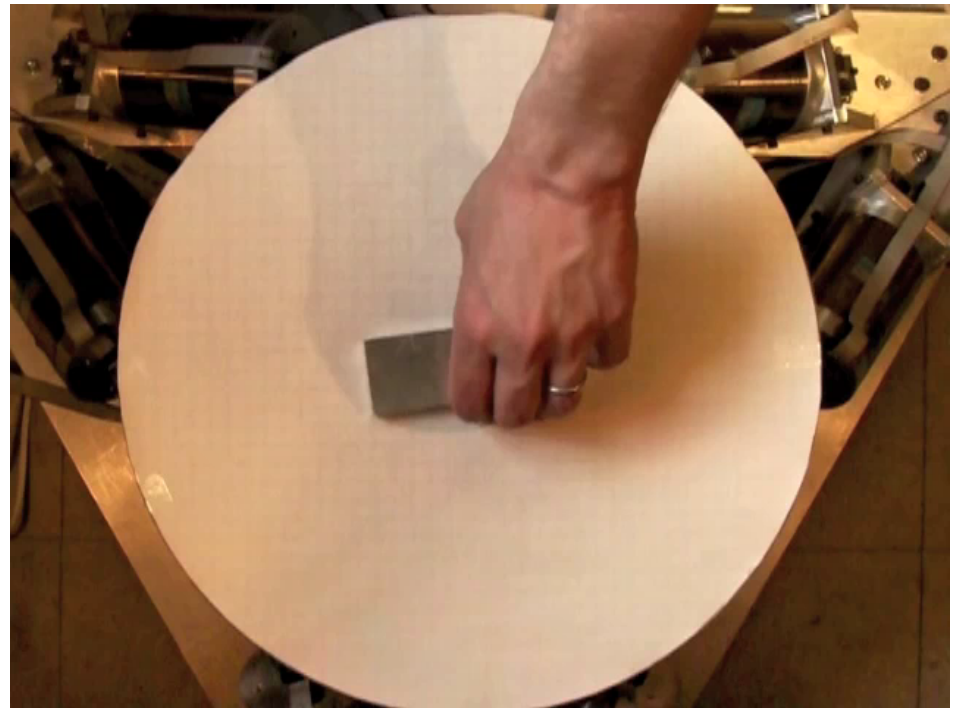
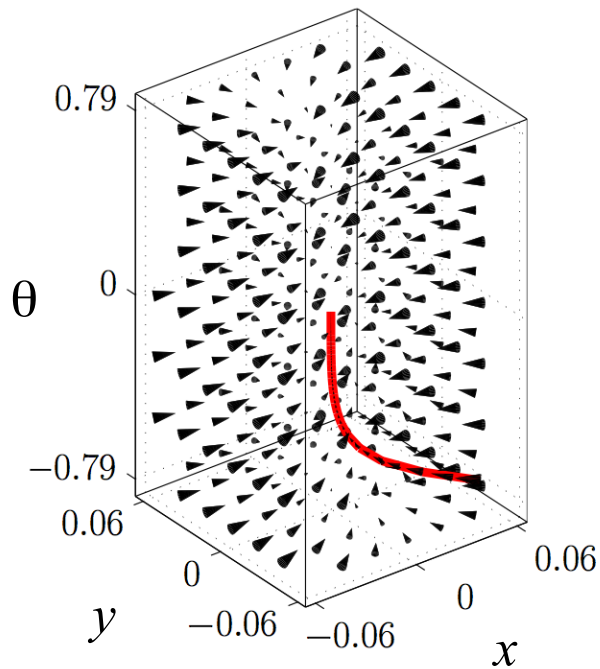
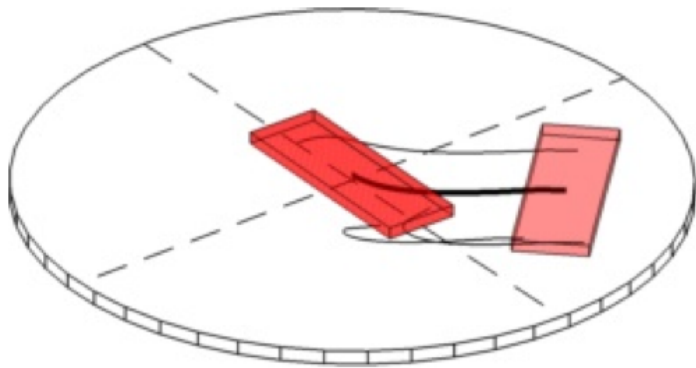
(g) Whirlpool



$$\begin{aligned} \ddot{p}_x &= 10 \sin(60\pi t) \\ \ddot{p}_y &= 10 \sin(60\pi t + \frac{1}{2}\pi) \\ \alpha_x &= 100 \sin(60\pi t + \frac{3}{2}\pi) \\ \alpha_y &= 100 \sin(60\pi t) \end{aligned}$$

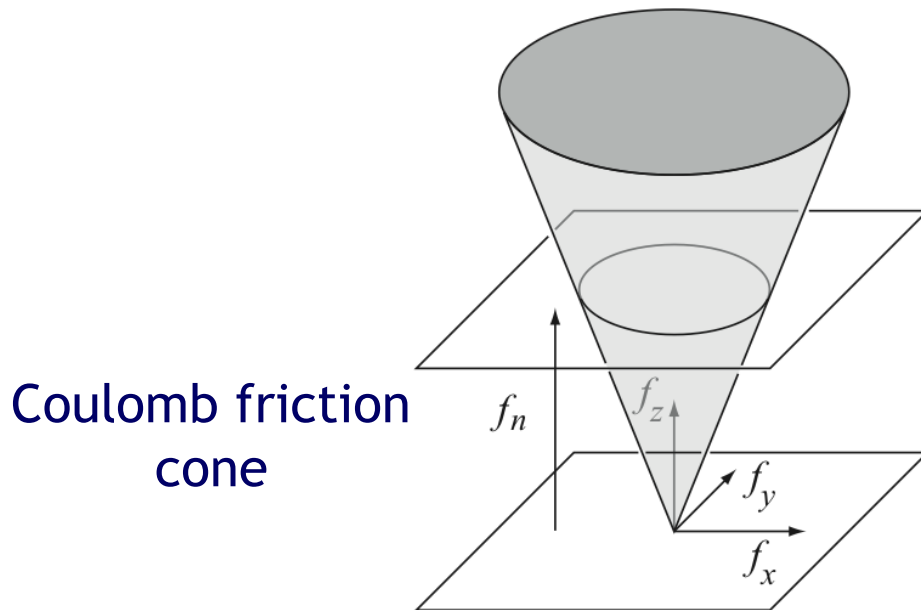
$$\mathbf{v}_a \approx \begin{bmatrix} -0.22x + 0.36y \\ -0.36x - 0.22y \end{bmatrix}$$

Extension: 3D Velocity Field

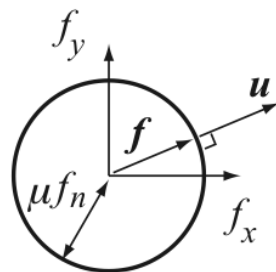


a sink field that uniquely positions and orients a part,
a la MEMS programmable vector fields
(Bohringer and Donald, Lamiroux and Kavraki)

Extension: Generalized Friction



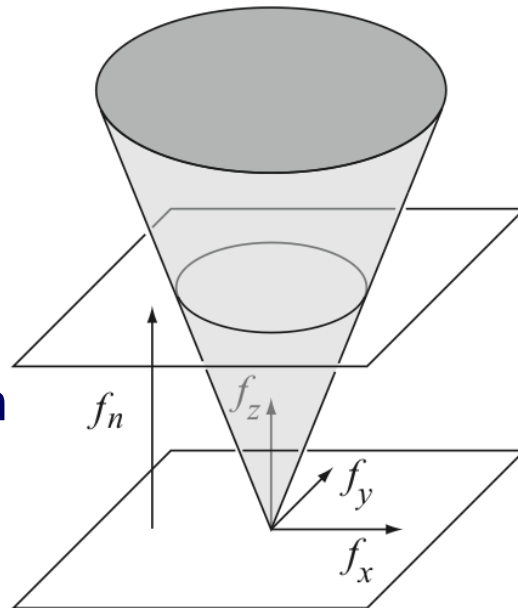
limit curve (LC) of possible friction forces at the specified normal force



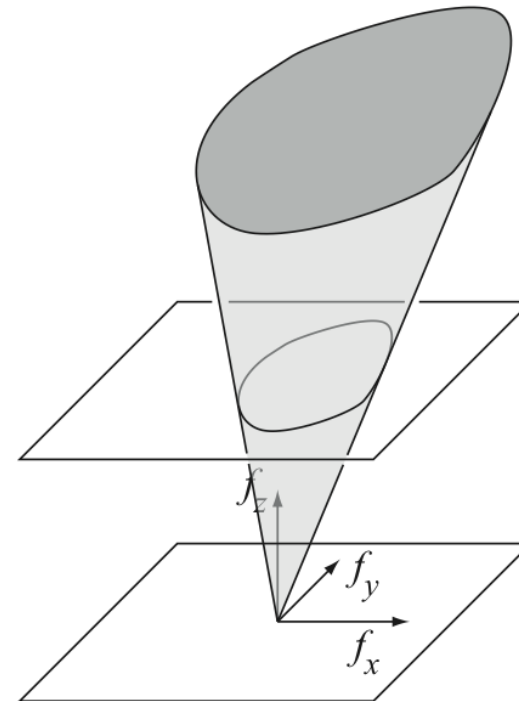
u sliding direction of support plane
 f force applied by support plane

Extension: Generalized Friction

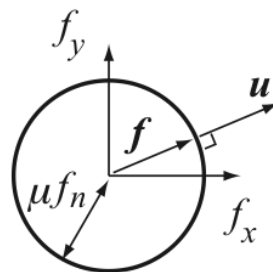
Coulomb friction cone



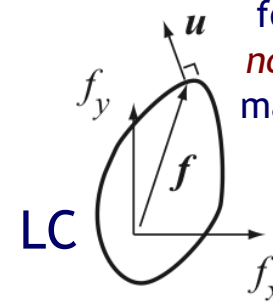
generalized *anisotropic* friction cone



limit curve (LC) of possible friction forces at the specified normal force

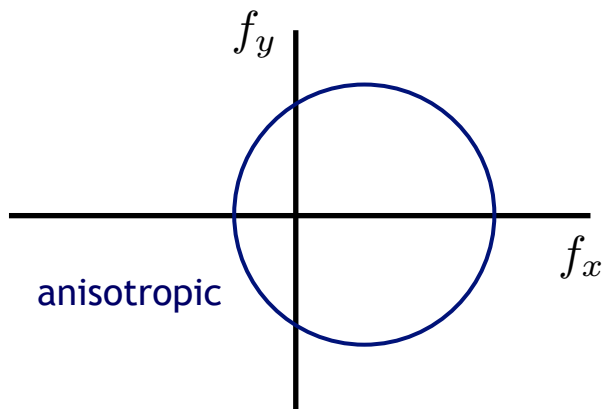
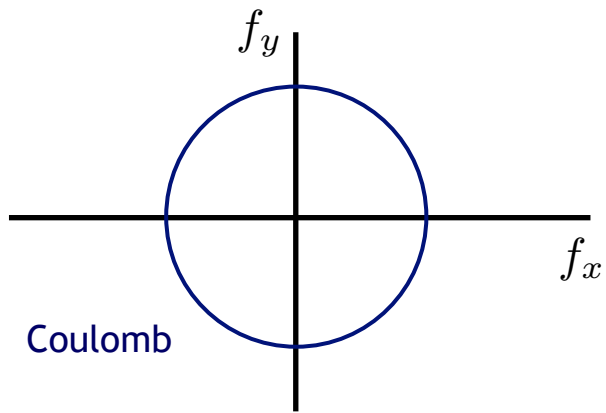


force and velocity satisfy *normality* at LC due to the maximum power inequality (Goyal, Ruina, Papadopoulos)

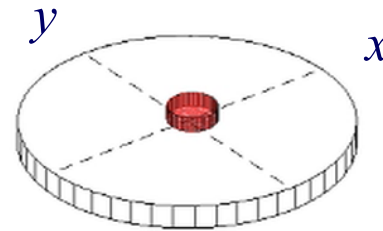
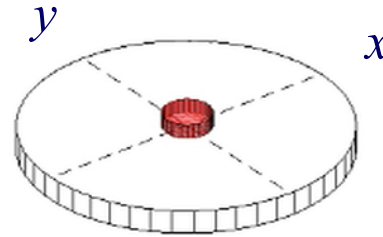


Linear Conveyance

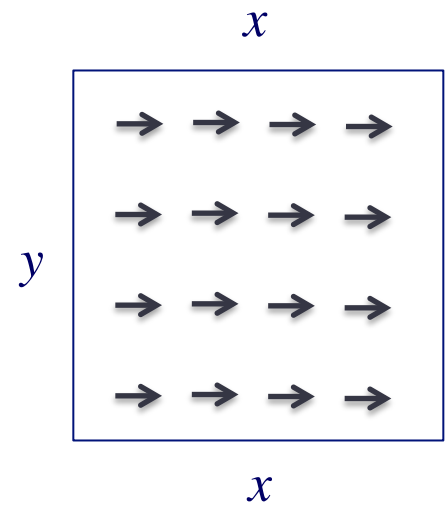
limit curve



sinusoidal plate motion

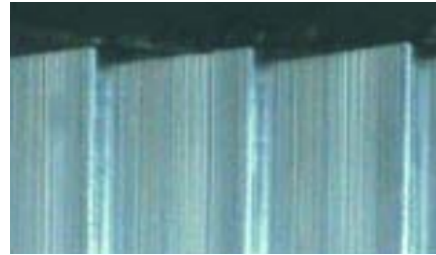


velocity field



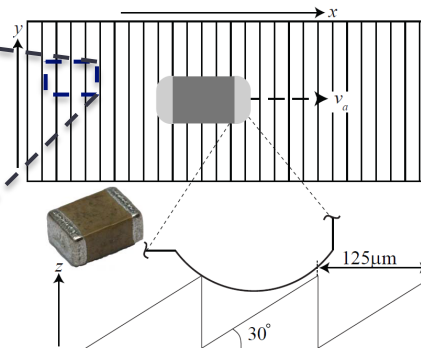
Extension: Generalized Friction

surface mount capacitor
on textured surface

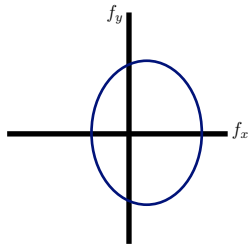


sawtooth profile surface

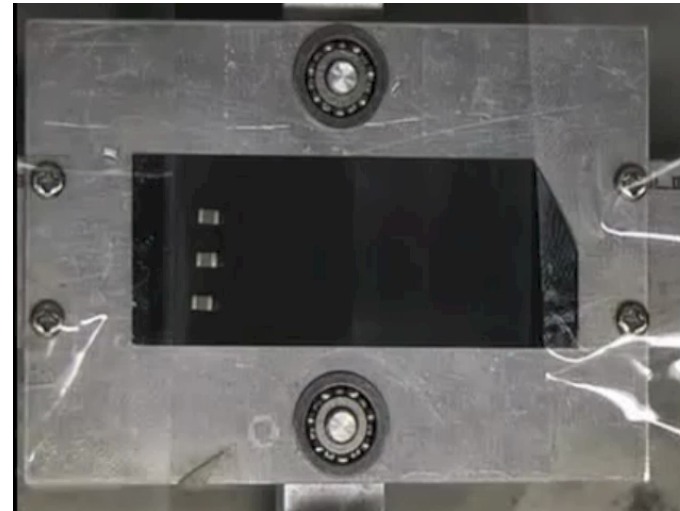
top view



side view



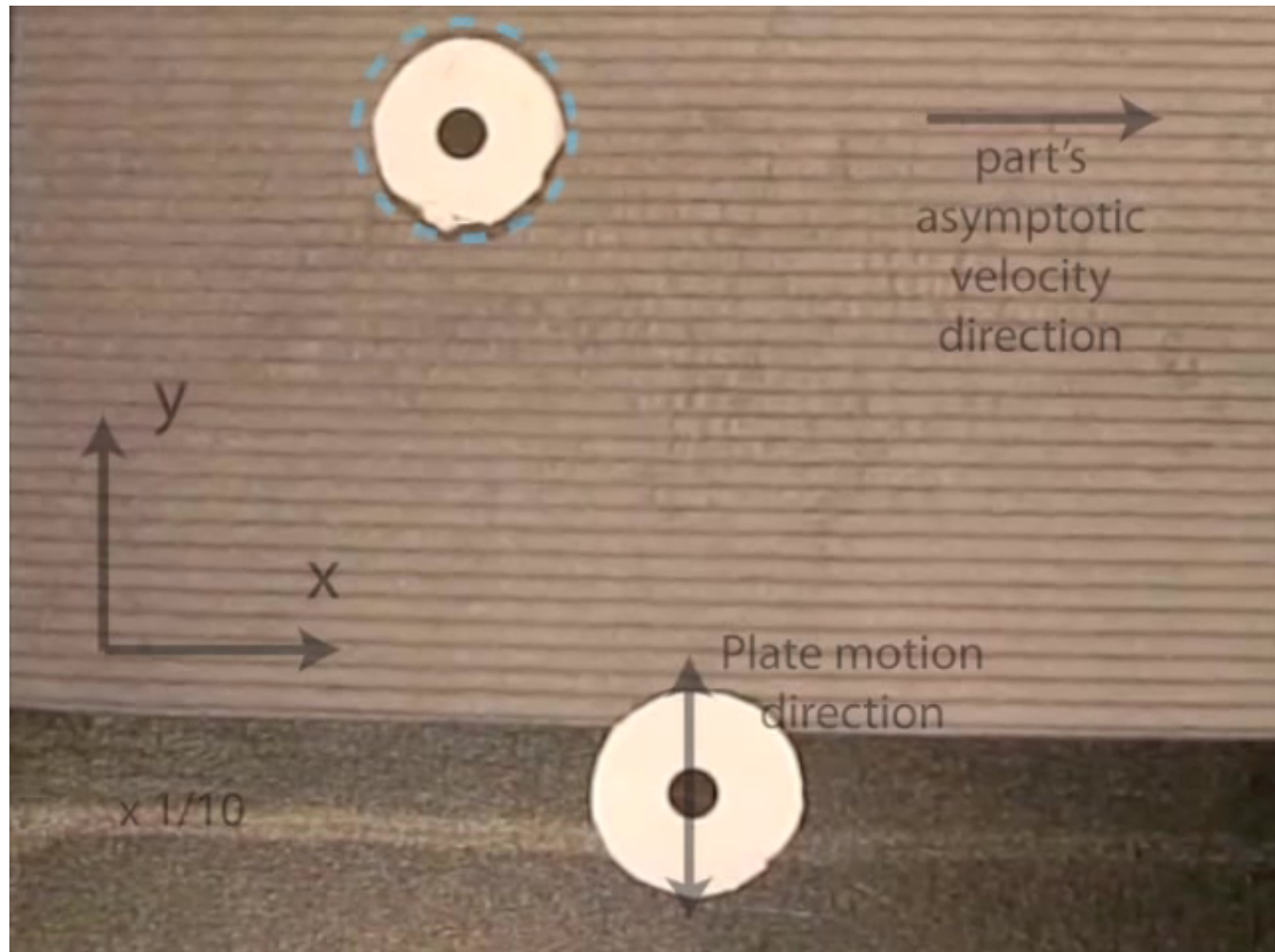
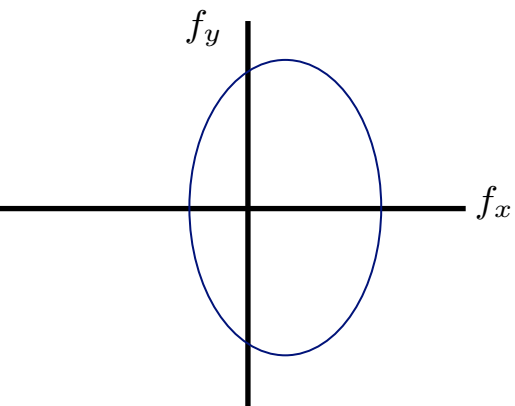
approximate anisotropic
friction limit curve



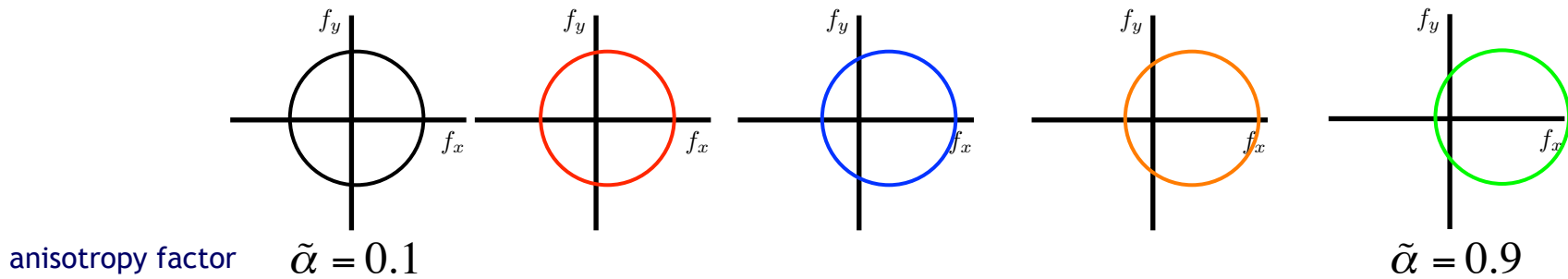
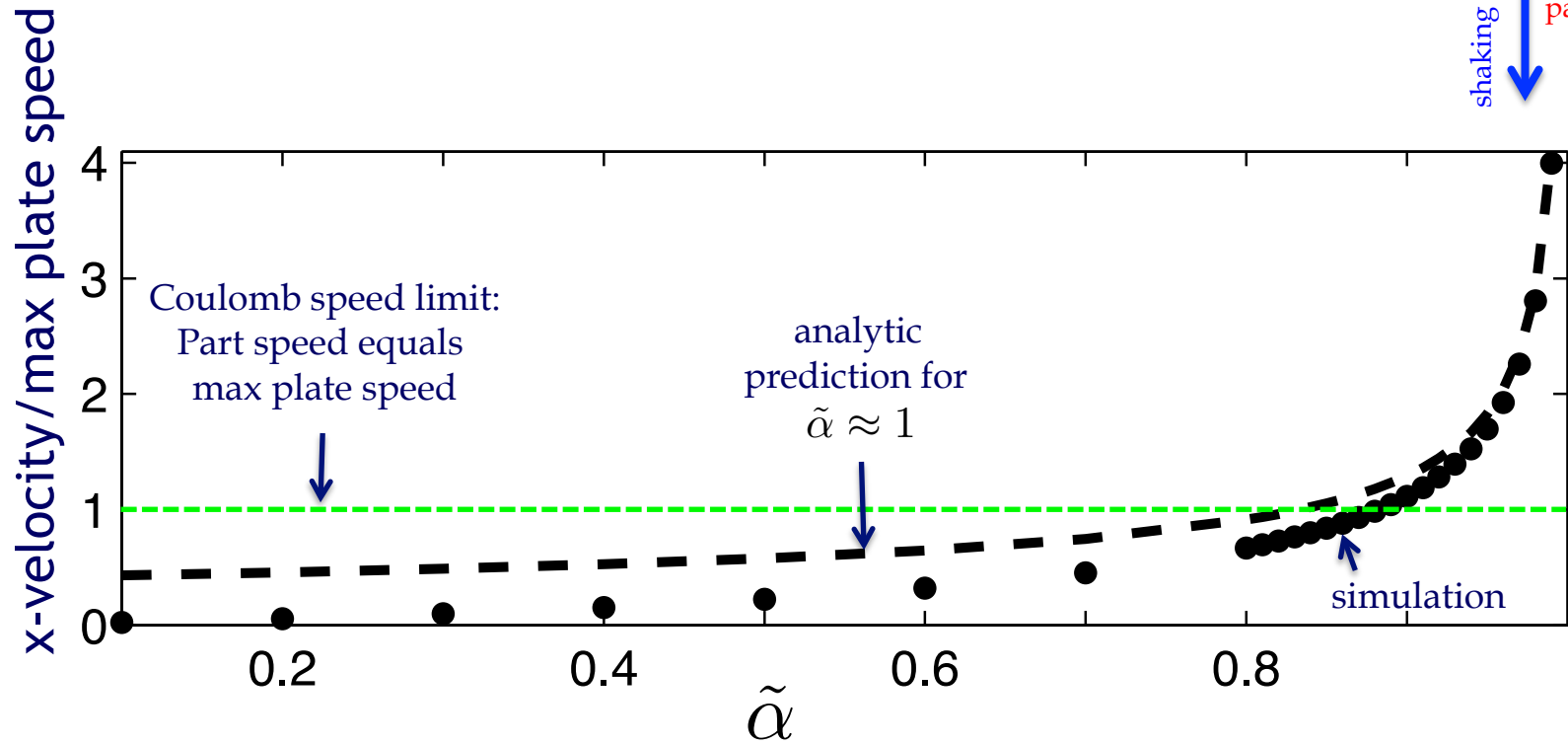
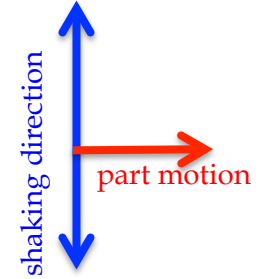
Mitani, Sugano, and Hirai 2006

Example: Corduroy Fabric

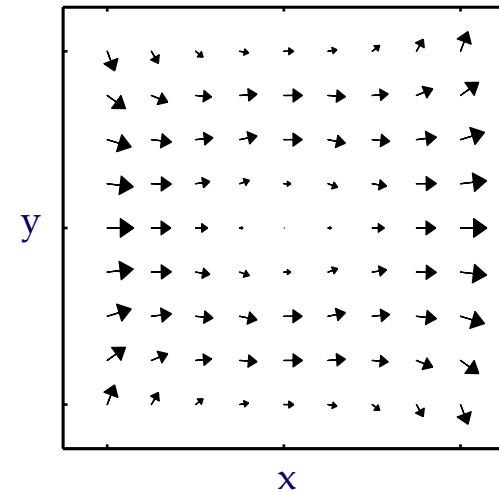
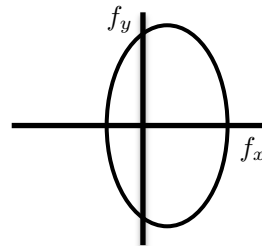
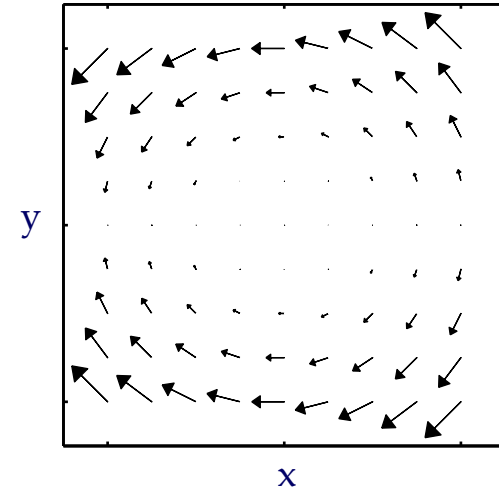
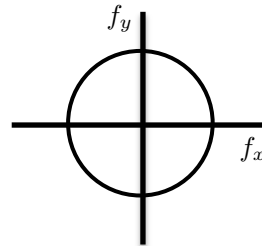
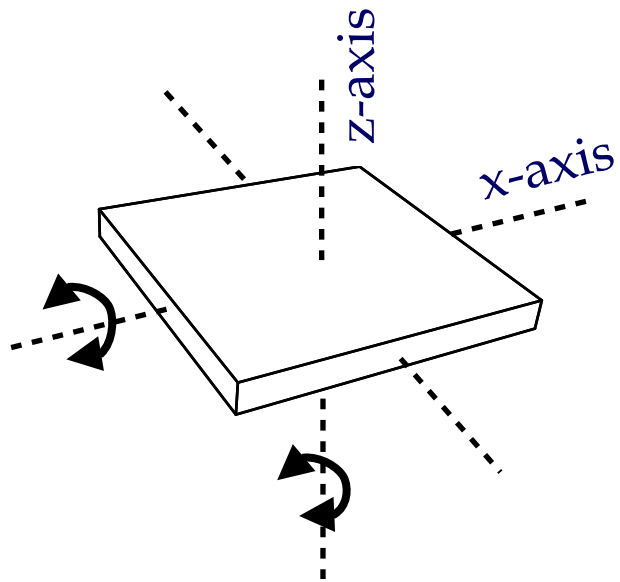
Overhead view of plate



Unbounded Part Speeds!



Morphing Velocity Fields



anisotropy adds nonlinear bias

Challenges

programmable motion surfaces

- texture design for desired anisotropic friction
- self-assembly
- impact for 6 DOF manipulation
- integration into flexible manufacturing cells

hybrid nonprehensile manipulation

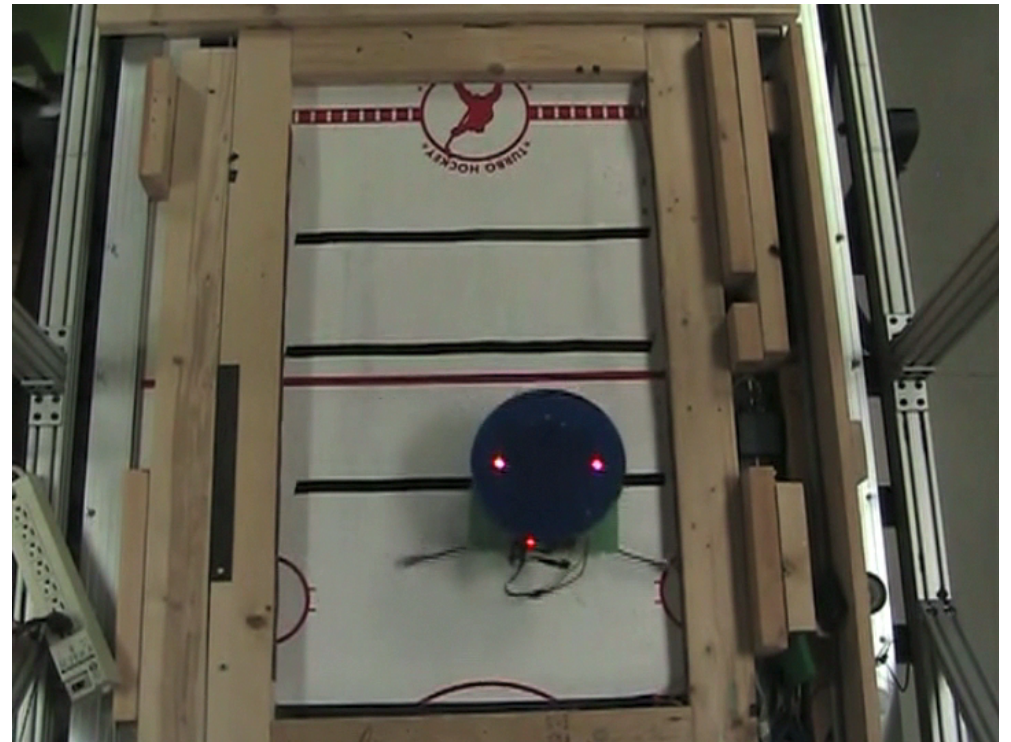
- state estimation: integrating far-field (vision, depth), near-field (electrosense, capacitive), and contact (tactile) data in real time
- library of primitives: motion planning and control
- automatic sequence planning with uncertainty
- estimating reachable sets

unified approach to dynamic manipulation and locomotion

Parkour



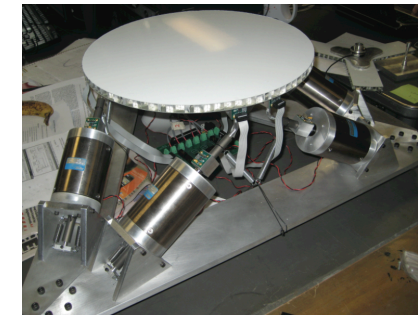
ParkourBot
with Degani, Feng, Long, Brown,
Choset and Mason



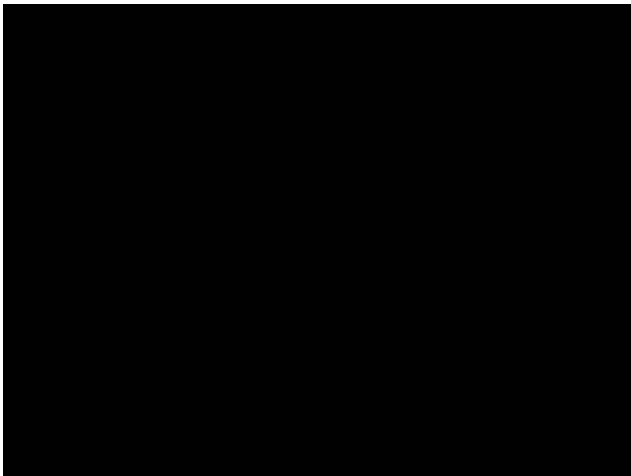
Congratulations Mark! (and Matt!)



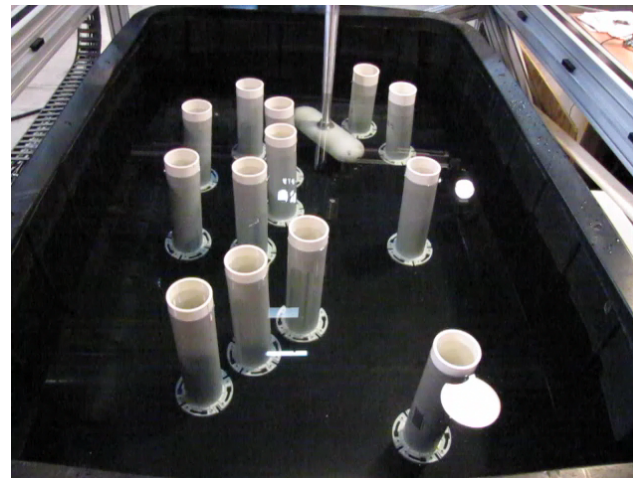
parkour, dynamic locomotion



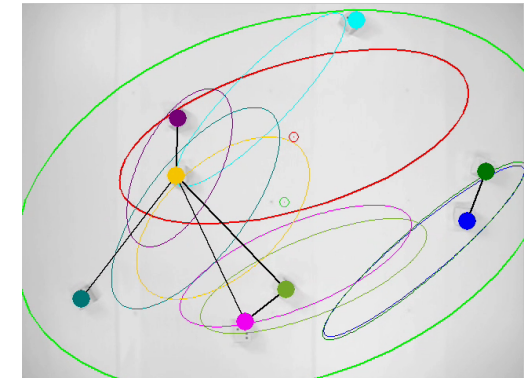
robot manipulation



restoration of function to paralyzed subjects by functional electrical stimulation



bio-inspired sensing: electrosense



self-organizing swarms of mobile sensors